

Influence of important parameters on the adsorption of diclofenac sodium by an environmentally friendly eucalyptus wood biochar and optimization using response surface methodology

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Received 9 January 2021; Accepted 6 May 2021

ABSTRACT

Diclofenac sodium is a pharmaceutical that is extensively prescribed and consumed worldwide. Consequently, its release into water bodies has become a global concern, as it poses ecotoxicity, leading to severe public health and environmental problems. A literature research was performed to find a low-cost adsorbent with cationic characteristics that could be used to remove anionic contaminants from water, such as diclofenac sodium. In view of the above, this work aimed to investigate diclofenac sodium (DFS) removal using eucalyptus wood biochar (EWB) through the adsorption process. EWB was characterized by various techniques to obtain information regarding its surface charge, morphology and functional groups. Scanning electron microscopy displayed a porous surface, and Fourier-transform infrared spectroscopy showed a notable number of functional groups on the EWB surface. Brunauer-Emmett-Teller presented an $A_{\scriptscriptstyle BET}$ of 619.35 m² g⁻¹ and the point of zero charge was 7.98. The influence of pH, contact time, initial concentration, and temperature of DFS were studied in batch tests. Box-Behnken design was used in surface response methodology to optimize the process conditions and obtain the maximum adsorption capacity, which was found to be 42.08 mg g⁻¹, reached in 6 h, showing a good performance. Kinetic data best fit the pseudo-second-order model and equilibrium data were in better agreement with the Sips model, indicating monolayer adsorption. The thermodynamic study demonstrated the adsorption process was spontaneous and endothermic. Considering the high efficiency evidenced in this study, low cost for production and the adsorbent being a renewable source, EWB is a promising material with the potential to remove DFS from water.

Keywords: Water treatment; Diclofenac sodium; Biochar; Adsorption; Box-Behnken design

1. Introduction

In recent decades, contamination of natural resources has become increasingly threatening to public health and the environment [1]. Various emerging contaminants such as pharmaceuticals, personal care products and veterinary drugs have been detected in surface water, groundwater and water supplies, posing threats to the environment due to their ability to cause various undesirable effects [2,3].

Amongst emerging contaminants, diclofenac sodium is a non-steroidal anti-inflammatory drug used worldwide

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since it relieves analgesic, arthritic and rheumatic pain [4]. As an excessively used drug, diclofenac sodium (DFS) has been frequently found in the environmental matrix in surface water and groundwater at low concentrations [5]. Its presence is responsible for causing toxic effects on bacteria, algae, and several studies have also reported physiological changes in animals at low concentrations [6,7]. Thus, it is necessary to develop, study and search for more efficient methods to remove a pollutant such as DFS from water and wastewater.

Several treatment techniques can be used to reduce or even eliminate the presence of these contaminants in bodies of water and among them, techniques such as ozonation [8], membrane separation processes [9], advanced oxidation [10], coagulation [11], and biological degradation processes have been widely used for water and wastewater treatment. Although these methods have shown efficiency in contaminant removal, they have several drawbacks, such as toxic residual products [12]. On the other hand, the adsorption process is considered a promising technology for emerging contaminant removal due to its efficiency, simplicity, flexibility in operation and design, and economic affordability [13,14]. Besides that, the adsorption process meets the environmentally friendly requirements of green chemistry due to its low sludge production, low cost, non-toxic products and regeneration capability [15,16].

Many adsorbent materials have been used for contaminant removal, such as chitosan, zeolites, clay, and even waste and low-cost adsorbents such as sludge, fly ash, etc. [17]. Although different types of adsorbents have been studied, activated carbon and biochar are still outstanding alternatives to eliminate organic compounds [18,19]. Their characteristics involve great specific surface area, high porosity and adsorption capacity, the effectiveness of contaminant removal and low specificity [19,20].

Commercially available activated carbons have been utilized in several studies for water treatment, but these activated carbons may hinder the process due to their high cost [7]. Thus, for the purpose of reducing the use of highcost activated carbons, the use of alternative adsorbent materials has been reported because of their high selectivity, great removal performance, and low cost [21]. Thus, biochar has emerged as an advantageous and environmentally friendly material, manufactured at low cost for many purposes, such as pollution minimization, climate change mitigation, bioenergy utilization and biomaterial waste management [22,23]. The alternative cheap materials searched for include peat, tree, eucalyptus barks, soil, rice husk, wood, etc [24].

The Brazilian forestry sector represents a worldwide reference and shows the highest wood productivity in the world. Amongst the 7.83 million ha of the total area of trees planted for industrial purposes, eucalyptus plantations occupy 5.7 million ha [25]. In Brazil, the unused agricultural waste products represent widely available and environmentally friendly materials that have great potential as adsorbents for water and wastewater treatment. Applying these waste products in adsorption processes allows a better management of them and helps find a solution for contaminant removal in the water system [21]. Despite the diversity of studies reported in the literature utilizing activated carbon to remove diclofenac sodium from water, the use of eucalyptus wood biochar has not yet been reported. In this sense, this study aimed to explore the adsorption of diclofenac sodium in aqueous solutions by batch testing, using eucalyptus wood biochar as an adsorbent. The adsorption process was investigated through pH effect, contact time, initial drug concentration, and temperature. Box–Behnken (BBD) in response surface methodology (RSM) was utilized to optimize the maximum adsorption capacity. Finally, kinetic, equilibrium and thermodynamic studies were performed.

2. Materials and methods

2.1. Reagents

Diclofenac sodium ($C_{14}H_{10}C_{12}NNaO_2$) was purchased in Curitiba (Brazil) and Table S1 shows its characteristics and properties. Eucalyptus wood biochar was provided by Carbomafra SA. The material was crushed, sifted using a set of Tyler Sieves, and dried at 373 K for 24 h. Eucalyptus wood biochar (EWB) was used in this study with a particle size of 0.25 mm.

2.2. Adsorbent characterization

EWB was characterized by physicochemical and structural characteristics. The particle size was found by placing 20 g of EWB on a series of Tyler Sieves and mechanically shaking them for 5 min (Bertel VP-01). After this, the sieves were separated and the remaining EWB on each sieve was calculated. Finally, each adsorbent weight obtained was converted to a percentage of the total retained on each sieve.

Textural characterization was performed through N₂ adsorption/desorption isotherms at 77 K through a Quantachrome Gas Sorption Analyzer (Nova 2000) and the software NovaWin. The samples were degassed under vacuum at 363 K for 6 h. Brunauer–Emmett–Teller (BET) and Barrett–Joyner–Halenda methods were used to calculate the specific surface area and obtain the average pore volume and diameter, respectively.

Through scanning electron microscopy (SEM) Tescan VEGA3 LMU, it was possible to analyze the adsorbent morphology. The structural characteristics were studied and analyzed through X-ray diffraction (XRD) with the Shimadzu XRD-7000, performed in the 2θ ranging from 5° to 120°, and Raman spectroscopy using the WITec Alpha 300R, with a wave excitement of 531.973 nm and integration time of 1.09. Fourier-transform infrared (FTIR) spectra were obtained to explore the chemical groups on EWB, using a Varian 640-IR, ranging from 400–4,000 cm⁻¹ and with a resolution of 4 cm⁻¹.

The point of zero charge (pH_{pzc}) was performed in accordance with the methodology proposed by Regalbuto and Robles [26], in which 50 mg of EWB was prepared and mixed with 50 mL of distilled water under various pH conditions (MS Tecnopon®) ranging from 2 to 12. For pH adjustments, HCl and NaOH 0.1 mol L⁻¹ solutions were used. The samples were agitated at 200 rpm for 24 h at 298 K and then centrifuged at a speed of 2,400 rpm for a period of

20 min. After this, the pH was measured again and the pH_{pzc} was obtained through the plot of a pH_{final} × pH_{initial-final} graph.

2.3. Adsorption studies

The experiments were executed as batch studies. Diclofenac sodium stock solution (100 mg L⁻¹) was prepared in ultrapure water (MegaPure) and diluted to different concentrations for the experiments. After this, 50 mL of each DFS concentration was added to 100 mL amber bottles containing a certain amount of adsorbent. The mixtures were added into a thermostatic shaker (Tecnal TE-4200) for a predetermined time. The mixtures were centrifuged (Fanem – Baby I 206-BL) at 2,400 rpm for 20 min and the samples were quantified in a UV-Vis spectrophotometer (Global Trade Technology UV-5100) at 279 nm.

2.3.1. Influence of pH

The effect of pH was tested adjusting different pH conditions from 4 to 9 in the solution containing the pharmaceutical (10 mg L^{-1}), utilizing 20 mg of EWB. The experiment was conducted for 6 h at 298 K.

2.3.2. Influence of contact time

To study how the contact time influences the process, 20 mg of EWB was added in a 10 mg L^{-1} DFS solution. The experiment was conducted with different contact times (from 0.5 to 12 h) at 298 K and the best pH condition was previously found.

2.3.3. Experimental design

The RSM by Box–Behnken design (BBD) was conducted to optimize three operation parameters: speed rate (rpm), initial DFS concentration (mg L⁻¹) and adsorbent dosage (mg), to maximize the DFS uptake. Each variable was varied at three levels (–1, 0 and +1), indicating low, medium and high. The BBD matrix is shown in Table 1. A total of 15 experiments were designed in this research using Eq. (1).

$$N = 2k(k-1) + C_n \tag{1}$$

where *N* is the number of experiments, *k* is the number of variables and C_n is the number of center points.

The experimental results were fit to a second-order polynomial equation that describes the response surface and expresses the variables' interactions. The 3D surface plots were used to analyze the adsorption performance and analysis of variance (ANOVA) tests were performed

Table 1

Independent variables and their levels for BBD

to analyze the significance of the model [22]. The statistical tests were performed through the software Minitab® 19.

After the experiments were performed, the best adsorbent dosage, pH, contact time, stirring rate and initial drug concentration were chosen to conduct the following experiments for the modeling studies.

2.3.4. Influence of initial DFS concentration and temperature

To perform this test, 10 mg of EWB was mixed with the DFS solution containing different concentrations (3–21 mg L^{-1}) at various temperatures (295, 305 and 315 K). The experiment was evaluated using the best conditions from the previous studies and the best conditions obtained in BBD.

2.4. Adsorption modeling

Kinetic, equilibrium and thermodynamics were investigated through adsorption modeling to explain the characteristics and behavior of DFS removal by EWB. The samples were agitated during different contact times (0.5–12 h) at 185 rpm and 10 mg of EWB was mixed using 15 mg L⁻¹ DFS solution at natural pH (5.5) and 298 K.

The isotherms were analyzed at three temperatures (295, 305 and 315 K) under the agitation of 185 rpm for 6 h, varying the initial drug concentration (2–20 mg L⁻¹) at natural pH and 10 mg of EWB. Origin® 2016 was utilized for data fitting. Eqs. (2) and (3) were used to calculate the adsorption capacities (q_t and q_r mg g⁻¹).

$$q_t = \frac{\left(C_0 - C_t\right)}{m} v \tag{2}$$

$$q_e = \frac{\left(C_0 - C_e\right)}{m} v \tag{3}$$

where C_0 and C_e (mg L⁻¹) are the initial (t = 0) and equilibrium DFS concentration; v (L) represents the solution of the volume and m (mg) is the mass of EWB.

The adsorption process was investigated through kinetic models: pseudo-first-order (PFO) [Eq. (4)] [27], pseudo-second-order (PSO) [Eq. (5)] [28] and intraparticle diffusion (ID) [Eq. (6)] [29].

$$q_t = q_e \left(1 - e^{-k_1 t} \right) \tag{4}$$

$$q_t = \frac{q_e^2 k_2 t}{1 + q_e k_2 t} \tag{5}$$

Independent variables	Symbol	Levels		
		Low (-1)	Center point (0)	High (+1
Stirring rate (rpm)	X_1	100	150	200
Drug concentration (mg L ⁻¹)	X_{2}	5	10	15
Adsorbent dosage (mg)	X_{3}	10	20	30

$$q_t = k_{id} t^{0.5} + C \tag{6}$$

where q_i and q_e (mg g¹) are the quantity of DFS adsorbed per unity of mass at the established time and at equilibrium, respectively; k_1 (h⁻¹), k_2 (g mg⁻¹ h⁻¹) and k_{id} (mg g⁻¹ h^{0.5}) are the pseudo-first-order, pseudo-second-order and intraparticle diffusion rate constants, respectively, and *C* (mg g⁻¹) is the intercept associated with the thicker boundary layer.

For the equilibrium study, Langmuir [30], Freundlich [31], Sips [32] and Redlich–Peterson [33] isotherms were employed through Eqs. (7)–(10) to analyze the equilibrium characteristics of adsorption.

$$q_e = \frac{q_m K_L C_e}{1 + K_L C_e} \tag{7}$$

$$q_e = K_F C_e^{1/n_F} \tag{8}$$

$$q_{e} = \frac{q_{\max}K_{S}C_{e}^{n_{s}}}{1 + K_{S}C_{e}^{n_{s}}}$$
(9)

$$q_e = \frac{K_{\rm RP} C_e}{1 + \alpha_{\rm RP} C_e^{\beta}} \tag{10}$$

where C_e (mg L⁻¹) is the solution concentration at equilibrium; q_m (mg g⁻¹) is the maximum adsorption possible; K_L (L mg⁻¹), K_F (mg g⁻¹)(mg L⁻¹)^{1/nF}, K_S (L mg⁻¹), and K_{RP} and α_{RP} (L mg⁻¹)^{β} are the Langmuir, Freundlich, Sips, and Redlich–Peterson constants, respectively; n_F and n_S are Freundlich and Sips constants for heterogeneity. The closer n_S is to zero, the more heterogeneous the system is ($0 \le n_S \le 1$) [34]

and β is the Redlich–Peterson exponent that lies between 0 and 1.

2.5. Thermodynamic study

Changes in the temperature can affect the nature of the process, along with its characteristics. The adsorption study was investigated at three temperatures (295, 305 and 315 K) through the thermodynamic parameters: Gibbs free energy change (ΔG , kJ mol⁻¹), enthalpy change (ΔH , kJ mol⁻¹) and entropy change (ΔS , J mol⁻¹ K⁻¹). Both parameters were obtained by the following equations:

$$\Delta G = -RT\ln K \tag{11}$$

$$\ln\left(K\right) = \left(\frac{\Delta S^{\circ}}{R} - \frac{\Delta H^{\circ}}{R}\right) \frac{1}{T}$$
(12)

where *R* (8.314 J mol⁻¹ K⁻¹) is the universal gas constant and *T* (K) is the absolute temperature. The thermodynamic equilibrium constant (K) was calculated using the best-fit isotherm model, according to the methodology described by Lima et al. [35].

3. Results and discussion

3.1. Adsorbent characterization

EWB was characterized by the particle size, SEM, N_2 adsorption/desorption isotherm, BET, FTIR, XRD, Raman spectroscopy, and pH_{pzc} . Fig. S1 shows the particle size distribution. For 5 min, almost 50% of the total adsorbent



Fig. 1. SEM images of EWB at a (a) 20 μm and (b) 5 μm scale.

weight passed 250 mesh; hence, the adsorbent particle size used for the following experiments was 0.25 mm. Fig. 1 illustrates through the SEM images that EWB presented a porous structure distributed across the entire material surface and may be effective to remove DFS.

Through the analysis of XRD patterns for EWB (Fig. 2a), it was possible to observe the obvious amorphous structure exhibited by the typical diffraction bands at 23.78° and 44.08°, which belonged to (002) and (101) planes of graphitic carbon [36]. This agrees with the patterns shown in Raman spectroscopy (Fig. 2b), which exhibited a strong G band around 1,600 cm⁻¹ and a D band around 1,350 cm⁻¹, representing the graphitic and disordered structure, respectively [37].

Fig. 3a illustrates the FTIR spectra, revealing the chemical groups present on EWB. The high peak at a wavenumber of 3,464 cm⁻¹ indicates free and associated hydroxyl groups (O–H) in alcohols, carboxylic, water and phenolic compounds on the EWB surface [38,39]. The band at 2,364 cm⁻¹ indicates ketone structures present on EWB [40,41]. The peak at 1,637 cm⁻¹ is associated with C=C stretching vibrations in aromatic rings and C=O bond in the carboxylic acid group [42]. The band at 1,385 cm⁻¹ indicates C=C stretching vibrations in aromatic rings and CH bonding also contributes to this peak [43,44]. The characteristic peak at 1,115 cm⁻¹ consists of OH and/or C–O vibrations [40] and the bands at 461 and 613 cm⁻¹ are attributed to the external CH bonding of aromatic rings [41,45].

Fig. 3b shows the N_2 adsorption/desorption isotherm and Table 2 presents the pore size characteristics. EWB showed a high surface area (619.35 m² g⁻¹) and a great size distribution of the pores, confirmed by SEM images (Fig. 1a and b). The N_2 adsorption/desorption isotherm showed high N_2 adsorption at low P/Po, indicating that EWB contains micropores [46]. However, according to Thommes et al. [47], it is also a type IVa isotherm with hysteresis, which means that the adsorbent is mesoporous, being in conformity with the pore characteristics shown in Table 2. The surface charges present on the EWB surface were investigated through its pH_{pzc} . Fig. 3c illustrates the plot $pH_{final} \times pH_{initial-final'}$ where EWB showed a pH_{pzc} of 7.98. This means that the EWB surface presents negative charges for values below $pH_{pzc'}$ and positive charges for values above $pH_{pzc'}$.

3.2. Adsorption studies

3.2.1. Influence of pH

Fig. 4 displays the study of the pH effect. DFS is considered a weak acid (pKa = 4.15) and poorly soluble in water in its unionized form [48]. This means that favorable interactions between EWB and DFS will occur for pH values between the pH_{pzc} and the pKa. The adsorbent characteristics (pH_{pzc} = 7.98) and the acidic characteristics of DFS (pKa = 4.15) indicate that DFS adsorption should be guaranteed for pHs below the adsorbent pH_{pzc}.

When the pH of a solution is below pKa, the DFS solubility in water decreases [49], so this experiment was performed ranging from pH 4 to 9. Fig. 4 shows that increasing the solution pH slightly decreases the DFS adsorption. According to Guerra et al. [50], this happens due to the increase in the negative charge of EWB, as well as the number of deprotonated functional groups on the surface, such as -COO- and -O- [50,51]. In this case, electrostatic repulsion occurring between the pharmaceutical and the EWB negative surface can be observed. Additionally, the acidic groups of EWB observed in FTIR spectra (Fig. 3a) could favor the interaction with the polar functional groups present in DFS [12]. Hydrogen bonding between the carboxylic group of EWB and negative species of DFS could be occurring in the process [12,52]. As it can be observed in Fig. 4a, the change of the adsorption capacity as the pH changes are low, which means that both hydrogen bonding and Van der Waals forces could be playing a significant role in the adsorption process [53,54]. Bernardo et al. [52] also reported a similar behavior between the pH condition and the DFS uptake. The highest adsorption



Fig. 2. (a) XRD patterns and (b) Raman spectra of the EWB sample.



Fig. 3. (a) FTIR spectra of the EWB sample, (b) N_2 adsorption/ desorption isotherms of the EWB sample and (c) pH_{pzc} of the EWB sample at various pH conditions. Conditions: stirring rate = 200 rpm; temperature = 298 K; contact time = 24 h; adsorbent dosage = 50 mg.

Table 2 Textural characteristics of the EWB sample

Adsorbent	EWB
$A_{BET} (m^2 g^{-1})$	619.35
Average pore diameter (nm)	3.617
Pore volume (cm ³ g ⁻¹)	0.036

capacity was recorded to be at pH 5, which is an approximate value to the natural pH of the DFS solution (5.5). Therefore, the natural pH was adopted for the following experiments.

3.2.2. Influence of contact time

Fig. 4b illustrates the influence of various contact times (0.5–12 h) on the DFS adsorption. It is possible to observe a notable increase in DFS uptake at the early stage. This behavior occurs because of the availability of active sites and a higher possibility of adsorption. As the process progressed, the increase was slower because the quantity of available sites decreased. The highest adsorption capacity was found to be 20.86 mg g⁻¹ when the system reached equilibrium after 6 h, which means that there is no longer mass transfer between the fluid phase and the adsorbed phase.

3.2.3. Experimental design

Table S2 displays coded variables with their predicted and actual response results. The independent factors were stirring rate (X_1), drug concentration (X_2) and adsorbent dosage (X_3), and their individual behavior and interactions were studied by the BBD. Other parameters such as temperature, contact time, and pH were fixated. The adsorption capacity was the response and it was investigated through those parameters. The model generated the final quadratic polynomial equation [Eq. (13)] and Table S3 presents the results for the analysis of variance (ANOVA) test.

$$DFS_{removal} = -21.56 + 0.4212X_1 + 1.572X_2 - 0.252X_3 - 0.001245X_1^2 - 0.0521X_2^2 - 0.00023X_3^2 + 0.00369X_1X_2 - 0.00182X_1X_3 + 0.0074X_2X_3$$
(13)

The model was significant at a probability level of p = 0.05. ANOVA showed a high R^2 value (0.9912), implying that the developed model was accurate. This means that the regression model represented 99.12% of the experimental results and only 0.88% was not explained by this model [55]. The predicted vs. actual results plot for DFS uptake is depicted in Fig. S2. The plot showed a correlation coefficient of 0.9905, revealing a good correlation between the actual and predicted values. The predicted R^2 value (0.8658) and the adjusted R^2 (0.9754) were reasonably in agreement, indicating the reliability of the model [56]. Sood et al. [57] reported that the insignificant value of lack of fit (>0.05) is desirable because it reveals that terms left out of the model are not significant. The lack of fit value during this study was 0.081, suggesting that the developed model fit well.

Fig. 5 illustrates the three-dimensional (3D) response surface plots of DFS adsorption as a function of independent



Fig. 4. (a) Effect of pH in 6 h of contact time and (b) contact time at pH 5.5 (natural) of DFS adsorption on EWB. Conditions: stirring rate = 200 rpm; initial DFS concentration = 10 mg L^{-1} ; temperature = 298 K; adsorbent dosage = 20 mg.



Fig. 5. 3D plots showing the effects of (a) stirring rate and drug concentration (b) stirring rate and adsorbent dosage and (c) drug concentration and adsorbent dosage in the DFS adsorption on EWB. Conditions: pH = 5.5 (natural); temperature = 298 K.

variables. The plot verifies the interactive 3D effects of the dependent variable (DFS adsorption capacity) and three independent variables (stirring rate, drug concentration and adsorbent dosage), in which one variable is set constant in its center point (0). Fig. 5a shows the DFS adsorption capacity in relation to the stirring rate and drug concentration, with a constant adsorbent dosage. The adsorption capacity increases from 9.31 to 24.77 mg g⁻¹ by increasing the stirring rate and drug concentration. This happens because the increase in the initial drug concentration requires a higher amount of the drug to be adsorbed, raising the driving force from the concentration gradient [58] and increasing the stirring speed, thus enhancing the homogeneity to the mixture [59].

Fig. 5b depicts the relationship of the DFS uptake as a function of stirring rate and adsorbent dosage, with a constant value of drug concentration. The DFS adsorption capacity increases with an increase in the stirring rate but with a decrease in the EWB dosage (from 11.39 to 25.23 mg g⁻¹). The adsorption capacity represents the quantity of the DFS adsorbed by EWB per unit mass. Therefore, it tends to increase by using a smaller amount of EWB, since raising

the EWB dosage results in the instauration of the adsorbed sites [60,61]. Furthermore, interactions between the particles may occur, such as aggregation, which is a result of the high amount of adsorbent [60].

Finally, Fig. 5c shows the DFS adsorption capacity in relation to drug concentration and adsorbent dosage, with a constant stirring rate. The adsorption capacity increased from 7.17 to 30.51 mg g⁻¹ by increasing the concentration and decreasing the adsorbent dosage. This occurs because the solution contains a greater amount of adsorbate, which will fill all the available adsorbent sites, thus increasing the adsorption capacity. Hence, the maximum DFS uptake occurs for greater stirring rate and drug concentration, and for lower EWB dosage.

BBD and RSM were used to reveal the best conditions for the DFS uptake. The optimal conditions were 183.84 rpm for the stirring rate, 15 mg L⁻¹ for the drug concentration and 10 mg for the adsorbent dosage. These conditions showed a predicted adsorption capacity of 31.03 mg g⁻¹. A new experiment with the optimal conditions was conducted to validate the optimization and obtain the actual q_e value (31.78 mg g⁻¹). Table S4 shows the optimal conditions and the actual q_e value. The stirring rate was set to 185 rpm to benefit the process.

3.3. Adsorption study

3.3.1. Kinetic study

The kinetic modeling study helps to investigate and analyze the efficiency for pollutant removal [62], adsorption dynamics and how time affects the process [63]. With the optimal conditions obtained from BBD in Section 3.2.3 – Experimental design, the second study of contact time was performed for the kinetic modeling.

The second study of contact time was performed in order to compare the adsorption capacity before and after the application of the Box–Behnken design. Fig. 6a shows similar behavior to the study depicted in Fig. 4b. There was a rapid uptake increase in the first 4 h, with an adsorption capacity of 35 mg g⁻¹, which was 2.16 times higher than the one witnessed in Fig. 4b for the experiment performed without the optimal conditions (15.48 mg g⁻¹). After reaching the equilibrium in 6 h, the adsorption capacity increased from 20.42 mg g⁻¹ without the optimal conditions (Fig. 4b) to approximately 43.98 mg g⁻¹ with the optimal conditions (Fig. 6a). Table 3 presents the kinetic parameters regarding PFO, PSO and ID.

The standard deviation of residues (SD) was used to help comprehend the fitness of each model by dividing the SD of each model by the SD of the minimum value. The lesser SD values indicate a smaller disparity between the theoretical and experimental q values [64]. Fig. 6a and b illustrate the kinetic data regarding PFO, PSO and ID.

In Fig. 6a and Table 3, it is possible to observe that the R^2 coefficient and SD showed that the pseudo-secondorder model best fit the data, with the greatest determination coefficient and the lowest SD amongst the models. A small difference can be noted between the experimental and calculated values for the adsorption capacity. This most possibly happens because, according to Wong et al. [65], boundary layer effects could be occurring during the process. However, the R^2 value is still higher and the SD value is lower for the PSO model, which indicates that the PSO model best fits the experimental data. Although PFO and PSO models are traditionally utilized in adsorption studies, the most limiting mechanisms are the ones related to diffusion, such as external diffusion, boundary layer or intraparticle diffusion [66]. The intraparticle diffusion model determines the adsorption rate-limiting step. If the ID model takes part in the process, then the plot $q_t \times t^{0.5}$ will be linear, and if the line passes through the origin (C = 0), it means that this model controls the process [67].

Table 3

Kinetic parameters for DFS adsorption on EWB. Conditions: stirring rate = 185 rpm; initial DFS concentration = 15 mg L^{-1} ; pH = 5.5 (natural); temperature = 295 K; adsorbent dosage = 10 mg

Pseudo-first-order		Pseudo-second-order				
$q_{\rm exp}$ = 32.96 mg g ⁻¹						
$q_t (\mathrm{mg} \mathrm{g}^{-1})$	32.27	$q_t ({ m mg g}^{-1})$	37.39			
k_1 (h ⁻¹)	0.5980	k_2 (g mg ⁻¹ h ⁻¹)	1.980.10-2			
R^2	0.9405	R^2	0.9789			
SD	1.977	SD	1.178			
	Intraparticle	e diffusion				
$k_{\rm id1} ({\rm mg}~{\rm g}^{-1}~{\rm h}^{-0.5})$	10.91	$k_{\rm id2} ({\rm mg}~{\rm g}^{-1}~{\rm h}^{-0.5})$	1.142			
С	4.889	С	29.41			
R^2	0.9449	R^2	0.3195			
SD	1.574	SD	0.5567			



Fig. 6. Adsorption kinetic data for DFS on EWB for (a) pseudo-first-order and pseudo-second-order models and (b) intraparticle diffusion model graph of $q_t \times t^{0.5}$. Conditions: stirring rate = 185 rpm; initial DFS concentration = 15 mg L⁻¹; pH = 5.5 (natural); temperature = 295 K; adsorbent dosage = 10 mg.

The plot in Fig. 6b exhibited a multilinearity containing two linear regions with different slopes, suggesting multiple steps in the process. The first stage represents the transfer of molecules from bulk through the film of liquid containing a high initial DFS concentration and a vast number of available sites. Therefore, this is the fastest sorption stage [68]. The next stage involves intraparticle diffusion as the rate-determining step, so the process happens through small pores [69]. Besides, the regression line did not pass the origin ($C \neq 0$), indicating that ID is not the only rate-limiting step in this process [70].

3.3.2. Equilibrium study

According to Abdulhameed [71], studying the equilibrium is important because it explains the adsorption mechanism and the affinity between the adsorbent and adsorbate. Various temperatures were used to obtain the isotherms through Langmuir, Freundlich, Sips and Redlich–Peterson models. Fig. 7 depicts the isotherms and Table 4 presents the model parameters.

Fig. 7 illustrates the investigation of the adsorption capacity in relation to the initial DFS concentration, using EWB as an adsorbent at three temperatures (295, 305 and 315 K). An increase in the DFS adsorption was observed with the increase of initial DFS concentrations ranging from 3 to 21 mg L⁻¹. At low initial DFS concentration, the availability of adsorption sites was relatively high and the drug was easily adsorbed, whereas, at high initial DFS concentration, the number of available sites decreased. This happens because of the increase in the driving force from the concentration gradient since the increase in the uptake at higher initial DFS concentration is a result of the greater availability of DFS ions in the solution and then more sorption will occur [58,72]. Lastly, the maximum uptake was 42.08 mg g⁻¹, indicating a great efficiency for DFS removal.

Changes in temperature affect the diffusion molecules and change the equilibrium capacity of the adsorbent for a specific adsorbate [73]. Fig. 7 shows that the temperature had an important influence on DFS uptake, since the maximum adsorption capacity increased from 30.74 to 42.08 mg g⁻¹ while the temperature increased from 295 to 305 K, using the best initial DFS concentration obtained in Box–Behnken experimental design (15 mg L⁻¹). This behavior indicates an endothermic nature [74]. Table 4 presents the model parameters obtained for each isotherm.

The Sips isotherm best-fit the data for all temperatures, having the highest R^2 values. This most probably happens because of the complexity of the Sips equation, which better describes the heterogeneous surface [6]. Although the Redlich–Peterson isotherm also showed a good fit considering the high R^2 and low SD values, the Sips isotherm showed the best fit. This model predicts that for low DFS concentrations, the data follows the Freundlich model, whereas, for higher DFS concentrations, it follows the Langmuir model. The best fit for the Sips isotherm was reported in various studies, such as sludge-based activated carbons [75], modified biochar from *Moringa* seed powder [34], activated carbons and polymeric resin [76], and commercial organoclay [6].



Fig. 7. Adsorption isotherms for DFS on EWB at (a) 295 K, (b) 305 K and (c) 315 K. Conditions: stirring rate = 185 rpm; pH = 5.5 (natural); contact time = 6 h; adsorbent dosage = 10 mg.

Table 4

Model	Parameters	295 K	305 K	315 K
	$q_{\rm exp} \ ({ m mg g}^{-1})$	30.38	34.35	40.11
	$q_{\rm max} ({\rm mg \ g^{-1}})$	37.81	43.09	51.82
Langmuir	$K_L ({\rm Lmg^{-1}})$	0.3702	0.3855	0.3923
	R^2	0.9718	0.9759	0.9713
	SD	1.220	1.322	1.751
	K_F ((mg g ⁻¹)(mg L ⁻¹) ^{-1/nF})	13.35	15.13	17.80
Ensure dli ale	$n_{_F}$	2.928	2.843	2.700
Freunalich	R^2	0.8784	0.8865	0.8845
	SD	2.533	2.869	3.511
	$q_{\max} (\text{mg g}^{-1})$	33.13	37.44	43.45
	$K_{\rm s}$ (L mg ⁻¹)	0.3264	0.3543	0.3609
Sips	n _s	0.6935	0.6865	0.6253
	R^2	0.9857	0.9908	0.9952
	SD	0.8679	0.8164	0.7163
	$K_{_{\mathrm{RP}}} (\mathrm{mg}\;\mathrm{g}^{-1})$	9.993	12.41	14.81
	$\alpha_{\rm RP}$ (L mg ⁻¹)	0.1236	0.1523	0.1324
Redlich-Peterson	B	1.274	1.235	1.298
	<i>R</i> ²	0.9873	0.9869	0.9859
	SD	0.8158	0.9763	1.226

Isotherm parameters for DFS adsorption on EWB. Conditions: stirring rate = 185 rpm; pH = 5.5 (natural); contact time = 6 h; adsorbent dosage = 10 mg

The increase of the temperature caused both K_s and n_s constant values to rise, indicating the favorable behavior at higher temperatures [77]. The higher the K_s values are, the stronger the affinity is between EWB and DFS [78,79]. Increasing the temperature results in the raising of the K_s parameter, which means that the adsorption capacity is favorable at higher temperatures, evidencing the endothermic process. The n_s constant values (0.693, 0.686 and 0.625) suggest that the adsorption process closely resembles the monolayer model ($n_s > 0.5$) [79], indicating that the behavior is more similar to the Langmuir isotherm.

Comparing the classic isotherm models, it is possible to note that the Langmuir model best fit the experimental data, with an R^2 value closer to the unit and lower SD values, while for the Freundlich model, the R^2 values did not reach 0.9 and the SD values were higher than the other models. Furthermore, the adsorption capacity obtained through the Langmuir model was closer to the experimental value, showing conformity with the data obtained during the adsorption process. It can also be affirmed that the adsorption process of DFS on EWB occurs based on the Langmuir model, implying that the adsorption occurs as a monolayer mechanism on a homogeneous surface, which assumes that all sites are identical and limited, without any interaction between the adsorbed molecules [36,70].

The DFS adsorption capacity through the Langmuir model obtained in this study was compared to other studies found in the literature (Table 5).

The maximum adsorption capacity obtained in this study showed to be similar to some of the studies performed for DFS removal. Although the adsorption capacity obtained in this study using EWB as adsorbent was lower than some obtained in other studies using different adsorbents, such as sugar cane bagasse-derived activated carbon [81] and magnetic amine-functionalized chitosan [82], it was still better compared to other adsorbents, such as polymeric resin [76] and commercial organoclay [6]. Considering that a natural and renewable adsorbent was used (Eucalyptus wood biochar), the results obtained in this study showed that the adsorption process of DFS on EWB was efficient.

3.3.3. Thermodynamic study

Through the thermodynamic study, as well as its characteristics and parameters (ΔG , ΔH and ΔS), it is possible to explore the adsorption feasibility, capacity, and rate, as well as its nature and type [83,84]. Eq. (11) was employed to calculate ΔG and, by plotting the graph $\ln K_s \times 1/T$ obtained from Eq. (12), it was possible to determine ΔH and ΔS parameters through the regression and linear correlation coefficients, respectively. Table 6 presents the thermodynamic parameters. The negative ΔG values imply that the DFS adsorption on EWB is spontaneous with a great affinity between them [39]. Also, the increase in the temperature decreases the ΔG values, suggesting that the process is favorable at higher temperatures [85].

The positive ΔH value (3.97 kJ mol⁻¹) confirms the endothermic nature [86], supporting the results of the equilibrium study, since increasing the temperature will raise the DFS uptake. The ΔH magnitude obtained in this study (<40 kJ mol⁻¹) suggests that the DFS removal can be described by physical adsorption [87]. As discussed above in Sections 3.1 – Adsorbent characterization and 3.2.1 – Influence of pH regarding the FTIR analysis and the

Table 5

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L	angmuir ads	orption a	capacity	of DFS	using	r different	adsorbents
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Adsorbent	Temperature	q_m	K _L	R^2	Reference
	(K)	(mg g ⁻¹)	(L mg ⁻¹)		
	295	37.81	0.3702	0.9718	
EWB	305	43.09	0.3855	0.9759	This work
	315	51.82	0.3923	0.9713	
	288	25.47	0.005	0.96	
Commercial organoclay	303	34.06	0.207	0.92	[6]
	323	39.39	0.628	0.94	
	298	159.7	0.25	0.98	
Lignin-porous biochar containing graphitic carbon	308	165.9	0.52	0.96	[80]
	318	195.1	0.21	0.98	
	298	35.2	0.36	0.93	
Pristine biochar	308	37.4	0.33	0.96	[80]
	318	46.3	0.30	0.98	
Sugarcane bagasse-derived activated carbon	298	315.0	0.0987	0.989	[81]
Polymeric resin	298	36.90	0.084	0.9959	[76]
Magnetic amine-functionalized chitosan	303.2	469.48	0.021	0.958	[82]

Table 6

Table 0			
Thermodynamic	parameters for	DFS adsorption	on EWB

ΔG (kJ mol ⁻¹)			ΔH	ΔS
22°C	32°C	42°C	(kJ mol ⁻¹)	(kJ mol ⁻¹ K ⁻¹)
-28.16	-29.33	-30.34	3.97	0.109

influence of pH, hydrogen bondings and Van der Waals forces can be mentioned as the main adsorption mechanisms for DFS adsorption on EWB. These are considered physical and non-covalent interactions between the adsorbent and the adsorbate [88,89], agreeing with the enthalpy value (3.97 kJ mol⁻¹). Other interactions of a physical nature were pointed out as an adsorption mechanism for DFS removal [90]. The positive ΔS value (0,109 kJ mol⁻¹ K⁻¹) suggests that randomness in the solid-solution interface increases during the process [91], which means that the adsorbed molecules will gain more translational entropy than the adsorbate ions can lose, and the randomness of the system will remain [92].

4. Conclusion

Eucalyptus wood biochar was explored as a cheap material for DFS removal. SEM images showed a porous structure distributed across the surface. N, adsorption/desorption isotherm showed a high N2 adsorption, with a hysteresis loop, superficial surface area of 619.13 m² g⁻¹ and average pore size of 3.617 nm. Batch tests showed that the best pH condition was found to be 5, at a contact time of 6 h and a temperature of 315 K. For RSM, the optimal parameters were 183.84 rpm for the stirring rate, 15 mg g⁻¹ for the initial DFS concentration and 10 mg for the adsorbent dosage. As for the kinetic study, the pseudo-second-order model best fit the experimental data, and the Sips model best fit the data for the equilibrium study. Through the thermodynamic parameters, the adsorption process was spontaneous and endothermic. The maximum adsorption capacity obtained was 42.08 mg g⁻¹. Finally, EWB has shown effective results on DFS adsorption, which means that this adsorbent is a promising and economic alternative for DFS removal.

Acknowledgments

This work was supported financially by the Higher Education Personnel Improvement Coordination (CAPES) under Grant [88882.441557/2019-01] and National Counsel of Technological and Scientific Development (CNPq) under Grant [487115/2013-9].

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Supplementary information

Table S1 Characteristics and properties of DFS

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10.0

Table S4 BBD optimal conditions for DFS adsorption onto EWB C₁₄H₁₀Cl₂NNaO₂ Molecular formula 15307-79-6 Optimal Actual q_e Parameter Molecular weight (g mol⁻¹) 318.13^a condition (mg g⁻¹) Acid dissociation constant (pKa) 4.15^{a} Stirring rate (rpm) 183.8 Solubility in water (mg L⁻¹) 2,430^a Drug concentration (mg L⁻¹) 15.0 31.78 Molecule size (nm) $1.01 \times 0.719 \times 0.484^{b}$

Adsorbent dosage (mg)

^a[S1], ^b[S2]

CAS

Table S2

BBD matrix of the predicted and actual DFS adsorption onto EWB

Run	Stirring rate (X_1)	Drug concentration (X_2)	Adsorbent dosage (X_3)	Actual value	Predicted value
1	100 (-1)	5 (-1)	20 (0)	9.317	8.480
2	200 (+1)	5 (-1)	20 (0)	11.49	11.46
3	100 (-1)	15 (+1)	20 (0)	18.90	18.93
4	200 (+1)	15 (+1)	20 (0)	24.77	25.60
5	100 (-1)	10 (0)	10 (-1)	17.78	18.68
6	200 (+1)	10 (0)	10 (-1)	25.23	25.32
7	100 (-1)	10 (0)	30 (+1)	11.39	11.30
8	200 (+1)	10 (0)	30 (+1)	15.20	14.31
9	150 (0)	5 (-1)	10 (-1)	18.09	18.03
10	150 (0)	15 (+1)	10 (-1)	30.51	29.59
11	150 (0)	5 (-1)	30 (+1)	7.168	8.094
12	150 (0)	15 (+1)	30 (+1)	21.07	21.13
13	150 (0)	10 (0)	20 (0)	20.49	20.54
14	150 (0)	10 (0)	20 (0)	20.92	20.54
15	150 (0)	10 (0)	20 (0)	20.18	20.54

Source	DF	SS (Aj.)	MS (Aj.)	<i>F</i> -value	Prob. $> F$	
Model	9	565.694	62.855	62.59	0.000	Significant
X_1	1	46.592	46.592	46.39	0.001	Significant
X ₂	1	302.393	302.393	301.09	0.000	Significant
X_3	1	169.172	169.172	168.45	0.000	Significant
X_{1}^{2}	1	35.760	35.760	35.61	0.002	Significant
X_{2}^{2}	1	6.276	6.276	6.25	0.055	
X_{3}^{2}	1	0.002	0.002	0.00	0.967	
$X_1 X_2$	1	3.400	3.400	3.39	0.125	
X_1X_3	1	3.305	3.305	3.29	0.129	
X ₂ X ₃	1	0.544	0.544	0.54	0.495	
Lack of fit	3	4.747	1.582	11.54	0.081	Not significant
Pure error	2	0.274	0.137	*	*	-
Total	14	570.716				
$R^2 = 0.9912$						

Table S3			
Analysis of variance	(ANOVA) for DFS	adsorption onto) EWB



Fig. S1. Effect of EWB particle size.



Fig. S2. The actual and predicted plots for DFS uptake capacity onto EWB.

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