# Removal of methyl orange from aqueous solution by electrochemical process using stainless steel/PbO<sub>2</sub>-TiO<sub>2</sub> stable electrode

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#### **ABSTRACT**

Methyl orange (MO) belongs to the group of acid dyes with an azo chromophore. It is a toxic substance that harms human health and the environment. Therefore, it is very necessary to treat MO before discharged into environment. In this paper, the sol–gel TiO<sub>2</sub> nanoparticles were dopped into PbO<sub>2</sub> layer on stainless steel (SS) substrate by the cyclic voltammetry method. The obtained SS/PbO<sub>2</sub> TiO<sub>2</sub> composite electrode was used to remove MO from the aqueous solution. The effects of current density, initial pH, degradation time, and MO concentration were investigated. The results by X-ray diffraction showed that the β-PbO<sub>2</sub> co-existed with  $\alpha$ -PbO<sub>2</sub> in composite coating. TiO<sub>2</sub> particles have been successfully doped into the  $PbO<sub>2</sub>$  layer because of containing 0.3% Ti proven by energy dispersive X-ray spectroscopy examination. The optimal conditions for MO treatment were a current density of 1.75 mA cm<sup>-2</sup>, initial pH of 6, degradation time of 50 min, and MO concentration of 50 mg L<sup>-1</sup>. The decolorization efficiency reached 99.31%, indicating that the MO was almost completely removed in the aqueous solution by electrocatalytic oxidation method using the stable electrode  $SS/PbO_2$ -Ti $O_2$  as the anode.

Keywords: PbO<sub>2</sub>-TiO<sub>2</sub> composite; Electrocatalytic oxidation; Methyl orange; Colorant treatment

# **1. Introduction**

Along with economic development, the problem of environmental pollution is increasingly serious, including the problem of water pollution. One of the most common types of pollutants is dyes. Dyes have entered the water resources from different industries such as textile, food, cosmestic, plastic, paper and printing [1–3]. The wastewater of the industries cause serious environmental pollution and affect human health. If the content of dyes in water is high, it will affect the growth and development of aquatic species because the ability to regenerate oxygen and absorb sunlight

is reduced [4]. Among the dyes, methyl orange (MO) is also interested in research by many scientists because it is toxic to aquatic life and human health. MO  $(C_{14}H_{14}N_3NaO_3S)$ belongs to acid dyes group with stability azo chromophore (–N=N–). Generally, MO is difficult to remove due to high water solubility and low biodegradability [5]. Currently, there are many methods to removal dyes in wastewater such as adsorption [3,6], coagulation–flocculation [7], biological treatment [8], chemical adsoption [9], bioadsorption [10], sonophotocatalytic treatment [11], Fenton reaction [12], electrocoagulation [13], and electrocatalytic oxidation [1,14]. Each method has advantages and disadvantages as well.

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Biological treatment proven technology and cost-effective but it has some limitations such as requiring a greater time for functioning, a little flexibility in design and operation [15]. Adsorption methods convert pollutants into another form [12]. Coagulation and flocculation create a lot of sludge [3]. But the electrocatalytic oxidation method has many significant advantages such as easy operation, laboratory temperature and pressure, high degradation efficiency, and no secondary pollution generation [16–19]. However, besides these advantages, there are still some limitations such as the short life of electrodes and low surface to volume ratio [19]. The mechanism of oxidation organic matter can be described is as follows: First,  $H_2O$  discharged at the anode surface (AS) to create AS(OH•). Then, organics are oxidized by hydroxyl radicals  $AS(OH^{\bullet})$  to form  $CO_2$  and  $H_2O$  [1,20–22] describing the mechanism of electrocatalysis occurring simply on the electrode surface as shown in Fig. 1.

Parameters of reaction time, pH value, concentration of organic substances and current density all have great influence on the efficiency of the electrooxidation process [23,24]. However, the anode electrode material plays a very important role in the electrochemical process, contributing to improving the MO processing efficiency [1]. The anode materials used for the electrochemical degradation process must be inert ones such as  $G/\beta$ -PbO<sub>2</sub> [1], Ti/  $PbO<sub>2</sub>$  [25], Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>/PbO<sub>2</sub>-ZrO<sub>2</sub> [16], Nb/PbO<sub>2</sub> [18], G/  $Ti_4O_7$  [14], SS/2D-PbO<sub>2</sub> [26], Ti/SnO<sub>2</sub>-Sb/PbO<sub>2</sub>-TiO<sub>2</sub> [27]. Ti/  $SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>/PbO<sub>2</sub>-TiO<sub>2</sub>$  [28]. Thus, the PbO<sub>2</sub>-TiO<sub>2</sub> coating is mainly studied on the Ti substrate that has already been coated with another mixed oxide layer.  $PbO_2$ -Ti $O_2$  composite could be synthesized by various ways such as electrode position by constant current method [29–32] and thermal combined electrochemical technique [28,29]. In the combined method, the authors first synthesized the metal oxide layers (SnO<sub>2</sub>-Sb, SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>) on the substrate by thermal method, then continued to superimpose  $PbO_2$ -TiO<sub>2</sub> layers by electrochemical method. These composite electrodes have a more stable structure and longer life than the original PbO<sub>2</sub> electrode [28]. MO treatment efficiency reached 95.5% after 240 min processing, quite high compared to some other processing methods such as combining hydrodynamic cavitation and chlorine dioxide (90.5% after reaction time of 90 min) [33], and electrocoagulation (83.0% after 15 min processing) [13]. However, a fabrication of this



Fig. 1. Simulation of the MO decomposition pathway mechanism on the anode.

composite direct on stainless steel (SS) substrate by electrochemical method has not been mentioned much. Based on the literature review, there have been no reports on the SS/  $PbO_2$ -TiO<sub>2</sub> stable electrode fabricated by cyclic voltammetry (CV) method using for anode material to remove MO from wastewater. The potential scanning speed as well as the number of potential scan cycles are two parameters that have a great influence on the quality and thickness of the electrochemical coating [34]. Moreover, this synthesis method is both simple, easy to perform and less expensive because the composite layer is formed directly on the SS substrate in just one step. Therefore, the fabrication of  $SS/PbO_2$ -TiO<sub>2</sub> electrode was regarded in this study.

In this paper,  $SS/PbO_2$ -TiO<sub>2</sub> electrode was prepared by CV method at constant scan rate and with unchanged CV number. Then, the electrode was used to treat MO in wastewater by the constant current method. The optimal parameters such as current density, initial pH, degradation time and MO concentration in the treatment process were also investigated. Easy  $SS/PbO_2$ -TiO<sub>2</sub> stable electrode fabrication by CV method and very high MO processing efficiency are the highlights of this research.

# **2. Experimental**

# *2.1. Chemicals*

All chemicals were analytical grade from China (nitric acid (65%–68%), copper(II) nitrate trihydrate (>99%), sodium hydroxide (>99%), methyl orange (>99%)) and Germany (Lead nitrate (>99%), ethylene glycol (>99%)). Ti $O_2$  nanoparticles were performed in sol–gel form  $(50 \text{ g L}^{-1})$ .

# 2.2. Preparation and characterization of PbO<sub>2</sub>-TiO<sub>2</sub> composite *electrode*

Before synthesizing the  $SS/PbO_2$ -TiO<sub>2</sub> electrode, the SS substrate of  $0.283$  cm<sup>2</sup> needs to be cleaned and polished. It was first polished on sandpaper from 400 to 2000, then dipped in a washing solution (concentrated  $H_2SO_4$  plus  $K_2Cr_2O_7$ ) to remove impurities. Finally, the electrode was treated in 60 g  $L^{-1}$  NaOH solution for electrochemical polishing by CV method (scan rate of 200 mV  $s^{-1}$ , potential from  $-0.7$  to 0.5 V). PbO<sub>2</sub>-TiO<sub>2</sub> composite was synthesized directly on clean SS by CV method from a mixed solution (0.5 M  $Pb(NO<sub>3</sub>)<sub>2</sub>$ , 0.05 M Cu(NO<sub>3</sub>)<sub>2</sub>, 0.1 M HNO<sub>3</sub>, 0.1 M C<sub>2</sub>H<sub>6</sub>O<sub>2</sub>, and 2 g  $L^{-1}$  TiO<sub>2</sub>). The conditions for this step were scan rate of  $50 \text{ mV s}^{-1}$ ,  $300 \text{ cycles}$ , and voltage range from 1.2 to 1.7 V vs. Ag/AgCl, sat. KCl reference electrode.

The surface morphology of  $SS/PbO_2$ -TiO<sub>2</sub> composite electrode was examined by scanning electron microscope (SEM) on Hitachi S-4800 (Japan). Material properties were obtained by X-ray diffraction (XRD) and energy dispersive X-ray spectroscopy (EDS) on D8-ADVANCE (Germany) and Jeol JSM-6490 JED 2300 (Japan), respectively. The electrochemical property of this composite electrode was characterized by CV (0.5 M  $H_2SO_4$  measuring solution, potential region from 0.8 to 1.8  $\overline{V}$ , scan rate of 100 mV s<sup>-1</sup>) and potential polarization (scan rate of  $5 \text{ mV s}^{-1}$ , potential from –200 to 200 mV compared to open circuit voltage (OCP) methods.

#### *2.3. Treatment of MO and analytical method*

MO in water was treated on a three-electrode system, including counter electrode (platinum plate), working electrode  $(SS/PbO<sub>2</sub>-TiO<sub>2</sub>$  composite electrode), and reference electrode  $(Ag\overrightarrow{AgCl}$ , sat. KCl electrode). The electrolyte solution included  $0.08$  M  $\text{Na}_2\text{SO}_4$ , initial pH (varied from 5 until 11), and initial MO concentration (30, 50, 70, 90, and 110 mg  $L^{-1}$ ). The further parameters for MO degradation were current density (1.00, 1.25, 1.50, 1.75, and 2.00 mA cm–2), and treatment time (10, 20, 30, 40, 50, and 60 min). The volume of MO solution was 10 mL for each experiment. MO solution before and after the degradation were measured by UV-Vis on the S80 (England) to determine the removal efficiency (H). In our experience, the color absorbance only has good linearity in the low concentration range  $(2-10 \text{ mg } L^{-1})$ . Therefore, this concentration range was chosen to construct a calibration curve to detect the concentration of MO in solutions. Absorbance was read at 465 nm. If the color of the MO solution is too concentrated, it should be diluted before the UV-Vis measurement is performed to obtain more accurate results.

The *H* value was determinate according to the following equation:

$$
H = \frac{(C_0 - C_t)}{C_0} \times 100
$$
 (1)

where  $C_0$  is the initial MO concentration and  $C_t$  is the residual MO concentration of solution after a time of MO treatment.  $C<sub>t</sub>$  is determined using the previously established calibration curve.

The analysis of intermediates obtained from the degradation of MO was determined by high-pressure liquid chromatography-mass spectrometry (HPLC/MS) on the Agilent 6530 Accurate-Mass QTOF (United States). Oxidation– reduction potential (ORP) was measured by using Sension1 unit (HACH, USA). It describes the degree of MO solution treatment.

#### **3. Results and discussion**

# 3.1. Physical characteristics of PbO<sub>2</sub>-TiO<sub>2</sub> composite electrode

# *3.1.1. X-ray diffraction*

Fig. 2 is the XRD spectrum of  $PbO_2$ -TiO<sub>2</sub> composite. The diffraction peaks located at 2 $\theta$  of 25.5°, 32.0°, 36.2°, 49.0°, 52.1°, 54.1°, 59.0°, 62.5°, 62.5° and 66.8° are featured the  $\beta$ -PbO<sub>2</sub> form. The weak peaks located at 2θ of 30.0°, 49.5° and 56.0° demonstrated the presence of  $\alpha$ -PbO<sub>2</sub> form [18,26]. This shows that  $PbO<sub>2</sub>$  in the composite exists in both crystalline forms.

#### *3.1.2. EDS study*

The surface composition analysis of  $SS/PbO_2$ -TiO<sub>2</sub> composite electrode was performed by EDS spectrum. It is seen in Fig. 3 that Pb, O and Ti elements can be detected in the  $PbO_2$ -TiO<sub>2</sub> composite [29]. The composition of elements in the composite is shown in Table 1. The result of EDS analysis indicated that the  $TiO<sub>2</sub>$  was successfully doped into PbO<sub>2</sub> coating by the CV method thanks to the contribution of 0.3% Ti besides O and Pb.

# *3.1.3. SEM observation*

The surface morphology of  $SS/PbO<sub>2</sub>$  and  $SS/PbO<sub>2</sub>-TiO<sub>2</sub>$ composite electrodes was investigated by SEM as shown in Fig. 4. The results show that the  $PbO_2$  surface is smooth, while the composite surface shows roughness due to the presence of tiny  $TiO<sub>2</sub>$  crystals implanted in the PbO<sub>2</sub> layer [30]. In addition, we also see the surface morphology of coatings formed from particles with different sizes because



Fig. 2. XRD spectrum of  $SS/PbO<sub>2</sub>-TiO<sub>2</sub>$  composite electrode (synthesized by CV method at 50 m $\bar{V}$  s<sup>-1</sup>, 300 cycles).



Fig. 3. EDS spectrum of  $PbO_2$ -Ti $O_2$  composite (synthesized by CV method at 50 mV  $s^{-1}$ , 300 cycles).

Table 1

Rate of elements on the  $SS/PbO<sub>2</sub>-TiO<sub>2</sub>$  composite electrode (synthesized at 50 mV  $s^{-1}$ , 300 cycles)

Element	Weight (%)	Atomic (%)
O K	24.35	80.44
Ti K	0.30	0.33
Pb M	75.35	19.23
Total	100.00	100.00



Fig. 4. SEM images of SS/PbO<sub>2</sub> (left side) and SS/PbO<sub>2</sub>-TiO<sub>2</sub> composite (right side) electrodes (synthesized by CV method at 50 mV s<sup>-1</sup>, 300 cycles).

PbO<sub>2</sub> existed in  $\alpha$ - and β-modifications (orthorhombic and tetragonal, respectively) having different network parameters [35]. The particle size of  $PbO<sub>2</sub>$  on both coatings is almost the same and become compact together.

3.2. Electrochemical properties of SS/PbO<sub>2</sub>-TiO<sub>2</sub> composite *electrode*

#### *3.2.1. Cyclic voltammetry*

Fig. 5 shows the voltammograms of  $SS/PbO_2$ -TiO<sub>2</sub> composite electrode in  $0.5 \text{ M H}_2\text{SO}_4$  solution at a scan rate of  $100$  mV s<sup>-1</sup>. On the 1st cycle, there was no oxidation peaks appeared but two reduction peaks were found corresponding to both α and β-modifications of lead dioxide to lead sulfate at 1.16 and 1.23 V, respectively. This indicates that both α- and  $β$ -PbO<sub>2</sub> forms exist together in the coating after electrode fabrication. This result is consistent with the XRD analysis above. From the 2nd cycle, only one reduction peak appeared indicating that this is the reduction peak of β-PbO<sub>2</sub> to PbSO<sub>4</sub>. It increases following the CV number, however, its position was shifted lightly on the left side. From the 5th cycle the oxidation peaks demonstrated the formation



Fig. 5. Cyclic voltammograms of  $SS/PbO<sub>2</sub>-TiO<sub>2</sub>$  composite electrode in 0.5 M  $H_2SO_4$  at 100 mV s<sup>-1</sup> (composite electrode synthesized by CV method at 50 mV  $s^{-1}$ , 300 cycles).

of α- and  $\beta$ -PbO<sub>2</sub> at about 1.60 and 1.75 V, respectively [36]. They were clearly increasing with CV number.

# *3.2.2. Potentiodynamic polarization*

The potentiodynamic polarization curves of  $SS/PbO<sub>2</sub>$ - $TiO<sub>2</sub>$  composite and SS/PbO<sub>2</sub> electrodes in 0.5 M  $H<sub>2</sub>SO<sub>4</sub>$  solution is shown in Fig. 6 from which the value of exchange



Fig. 6. Potentiodynamic polarization curves of SS/PbO<sub>2</sub> and SS/PbO<sub>2</sub>-TiO<sub>2</sub> composite electrodes in 0.5 M H<sub>2</sub>SO<sub>4</sub> at 5 mV s<sup>-1</sup> in logarit (a) and in linear form (b) (composite electrode synthesized by CV method at 50 mV  $s^{-1}$ , 300 cycles).

current density of coating layers can be determined by the extrapolation of Tafel (Fig. 6a). If the exchange current density (ECD) is high, the surface of the electrode is more active [37,38]. This means that the both fabricated electrodes have a good catalytic ability for the electrochemical reaction occurring on their surface due to relatively high ECDs (61.8 and 53.4  $\mu$ A cm<sup>-2</sup> for PbO<sub>2</sub> and PbO<sub>2</sub>-TiO<sub>2</sub> coatings, respectively). Linear graph (Fig. 6b) show that the composite electrode has slightly worse anodic polarization, but better cathodic polarization than  $PbO<sub>2</sub>$  electrode.

#### *3.3. Treatment of MO*

#### *3.3.1. Research on MO decomposition mechanism*

MO is treated by electrocatalytic oxidation processing. It means that the electrodegradation occurs on the surface of  $SS/PbO_2$ -TiO<sub>2</sub> anode electrode. HPLC/MS analysis results show that MO is fragmented into intermediate fragments before being decomposed into  $CO_2$  and  $H_2O$  (Figs. 7 and 8). The electrochemical process can be described in detail below. The color of MO is mainly yellow thanks to the anion  $-$  SO<sub>3</sub>. The proposed reaction mechanism for MO electrodegradation can be occurred in two steps. First, the hydroxyl radicals (•OH) formed by direct oxidation of water according to Eq. (2). They are physically adsorbed on the anode surface (AS) and become very active [21,29,39,40], which can oxidize organic compounds to intermediates following Eq. (3).

$$
AS + H2O \rightarrow AS(^{\bullet}OH) + H^{+} + e^{-}
$$
 (2)

$$
AS(^{\bullet}OH) + MO \rightarrow AS + intermediates
$$
 (3)

Second, MO is an oxidizable organic compounds so that the hydroxyl radicals will attack the electron-rich site such as –N=N– to decompose it being phenolic compounds (Fig. 8). These compounds further oxidized to quinone, organic carboxylic acid, and final products  $(CO<sub>2</sub>$  and  $H<sub>2</sub>O$ ) [11,14,40] as Eq. (4).

$$
AS(^{\bullet}OH) + intermediate \rightarrow AS + CO_2 + H_2O + inorganic ions
$$
\n(4)



Fig. 7. Pathway of MO electrodegradation on anode electrode.

The OH radicals can be confirmed by tert-butanol as a quenching agent added to the MO solution before the electrochemical treatment begins. The results showed that the MO concentration after 10, 30 and 50 min of treatment reached 30.57, 20.60 and 13.53 mg  $L^{-1}$  in the presence of tert-butanol (0.08 M), respectively, higher than that of the solution without tert-butanol (27.53, 4.19 and 1.43 mg  $L^{-1}$ , respectively), from 50 mg  $L^{-1}$  initial MO concentration. It can be explained that some of the newly formed •OH radicals were quenched by tert-butanol [Eq. (5)] [41], so the ability to oxidize MO of the solution was less.

$$
^{\bullet}OH + (CH_3)_{3} COH → H_2O + CH_2C (CH_3)_{2} OH
$$
 (5)

# *3.3.2. The effect of current density*

Current density is a very important factor in the electrochemical oxidation process. In the paper, current density was used to remove MO from 1.0 to 2.0 mA cm<sup>-2</sup>. Fig. 9a shows absorbance sharply decreases when current density increase. Fig. 9b shows that with MO initial concentration at  $50 \,\text{mg}$  L<sup>-1</sup> and treatment time of 60 min, the removal efficiency were achieved 86.84%, 94.25%, 96.43%, 97.55%, and 97.60% at the current density of 1.0, 1.25, 1.5, 1.75 and 2.0 mA  $\text{cm}^{-2}$ ,

respectively. The removal efficiency raises as the current density increase until 1.75 mA  $cm<sup>-2</sup>$  (97.55%) and nearly unchanged at the current density of 2 mA cm–2 (97.60%). So current density of 1.75 mA cm<sup>-2</sup> was used for the following studies.

## *3.3.3. The effect of treatment time*

Different times (10, 20, 30, 40, 50 and 60 min) were applied to study the electrocatalytic MO degradation in solution (Fig. 10a and b). An increase in decolorization performance can be observed as the processing time is increased. However, the processing time increased from 50 to 60 min, the removal efficiency increased insignificantly at 97.15% and 97.55%, respectively. Therefore the optimal time for processing is 50 min.

#### *3.3.4. The effect of initial concentration*

The MO initial concentration  $(C_{0,MO})$  is also a factor affecting the oxidation process. Therefore, in this paper, the MO initial concentration was considered from 30 to 100 mg  $L^{-1}$ . As the  $C_{0MO}$  increased, the absorbance increased (Fig. 11a) and the removal efficiency decreased (Fig. 11b). The optimal concentration is 50 mg  $L^{-1}$  with the efficiency of 97.15%.

# *3.3.5. The effect of solution pH*

MO has two chemical structures corresponding to two different colors when the pH value of solution is different. If pH value is smaller than 4.4, MO has quinoid structure corresponding red color. When pH value is larger than 4.4, MO has azo structure corresponding yellow color [37]. Therefore, the effect of initial pH on MO degradation in wastewater was studied in the paper. The  $H_2SO_4$  and NaOH solutions were used to adjust the solution pH [18]. Fig. 12a shows the absorbance reduces when pH reduces until 6 and is almost unchanged at pH of 5. So the suitable initial pH is 6. As can be seen from Fig. 12b, when initial pH increase from 5 until 7 the removal efficiency is very high (>99%), higher than that published in previous work using  $PbO_2$ -TiO<sub>2</sub> nanocomposite [27,28] and others [9–14,33,42] (Table 2). It indicates that MO molecules are easily decomposed at this pH range, but pH value larger than 7, the removal efficiency decreases sharply. Therefore, to be consistent with practice, a pH of 6 is the most suitable for MO treatment.



Fig. 8. HPLC/MS chromatographs before and after degradation of MO ( $C_{\text{MO}}$  of 50 mg L<sup>-1</sup>, pH 6, current density of 1.75 mA cm<sup>-2</sup>).



Fig. 9. UV-Vis spectra of the treated solution with different current densities (a); colour removal efficiency and residual MO concentration after 50 min at different current density from MO concentration of 50 mg  $L^{-1}$  (b) at pH 7.

From the results obtained in Fig. 13, the MO removal efficiency achieved after 50 min for the  $SS/PbO_2$ -TiO<sub>2</sub> composite electrode is  $99.31\%$ , higher than that of the SS/PbO<sub>2</sub> electrode (98.86%).

#### *3.3.6. Kinetic study*

The study of reaction rates has important implications for chemical processes. Therefore, the kinetic of MO degradation is considered in our research. The pseudo-firstorder was applied to study the kinetics of MO decomposition with the following conditions: treatment time from 10 until 60 min, pH of 7, initial MO concentration of 50 mg  $L^{-1}$ , and current density of 1.75 mA cm–2. The pseudo-first-order for MO degradation can be written as Eq. (6) [23,43,44] below:

 $\ln \left| \frac{C_o}{C_t} \right| = kt$  $\left| \frac{C_o}{C} \right|$  $\vert = kt \tag{6}$ L  $\mathbf{1}$ *t*  $\mathbf{1}$  $0.8$  $^{\circ}$  20  $. 30$  $0.0$ å  $\ddot{a}$  $\theta$ .<br>An  $0.2$  $0.0$ 

where  $C$ <sub>*c*</sub> and  $C$ <sub>*t*</sub> are the MO concentrations before and after processing at time (*t*), respectively, and *k* is the constant of removal rate. The *k* can be determined from plot  $ln(C_{o}/C_{t})$  vs. *t* (Fig. 14). The *k* of 0.0838 min<sup>-1</sup> ( $R^{2} = 0.9855$ ) and  $0.022$  min<sup>-1</sup> ( $\bar{R}^2$  = 0.9684) were found for the first period (0–40 min) and the second period (40–60 min), respectively. The MO processing speed in both periods is relatively linear because  $R<sup>2</sup>$  is quite high. However, this result also shows that the MO processing occurring at the first 40 min is almost four times faster than in the next stage.

# *3.3.7. Consideration of the ORP*

As we know ORP is considered for indicating the level of MO solution treatment. The value of ORP can describe the quality of the solution, while the ΔORP between the inlet and outlet wastewater reflects the pollutant removal efficiency [45]. The higher the ORP value is, the better the



Fig. 10. UV-Vis spectra of the treated solution with different times (a); colour removal efficiency and residual MO concentration after different treatment time from MO concentration of 50 mg L<sup>-1</sup> at pH 7.



Fig. 11. UV-Vis spectra of the treated solution with different MO concentrations (a); colour removal efficiency and residual MO concentration after 50 min from different initial MO concentrations (b) at pH 7.



Fig. 12. UV-Vis spectra of treated solution with different pH (a); colour removal efficiency and residual MO concentration after 50 min treatment at different pH (b) from initial MO concentration of 50 mg  $L^{-1}$ .



Fig. 13. UV-Vis spectra of treated solutions using  $SS/PbO<sub>2</sub>$  and SS/PbO<sub>2</sub>-TiO<sub>2</sub> composite electrodes (treatment conditions: *C*<sub>0,MO</sub> of 50 mg L<sup>-1</sup>, pH 6, 50 min at current density of 1.75 mA cm<sup>-2</sup>).



Fig. 14. The plots of  $\ln(C_0/C_i)$  vs. MO treatment time *t*.

# Table 2

Comparison of MO treatment with some published researches

Operating condition	Treatment method	Removal efficiency	References
Initial MO concentration of 100 ppm and a sorbent dose of 0.05 g, pH 3, temperature of 30°C	Using polymeric chitosan-iso-vanillin	97.9% after 3 h contact time	$[9]$
Initial MO concentration of 20 mg L <sup>-1</sup> and pH 6	Using hog plum peel and mix-bacterial strains	92.0% after 60 min contact time	[10]
Initial MO concentration of 100 mg $L^{-1}$ in 1 g $L^{-1}$ synthesized nano-zinc oxide and $1.5$ g $L^{-1}$ sodium persulfate, pH 6.5	By sonophotocatalytic treatment with synthesized nano-zinc oxide	84.0% after reaction time of 60 min	$[11]$
[MO] = $5.4 \times 10^{-5}$ M, [Fe <sup>2+</sup> ] = $1.9 \times 10^{-4}$ M; $[H, O]$ = 2.93 × 10 <sup>-3</sup> M; pH = 2.79 at room tempera- ture	By Fenton reaction	97.8% after 15 min	$[12]$
Iron electrode (22.5 cm <sup>2</sup> ) as an active surface, current density of 64 A m <sup>-2</sup> , and pH 7.25	By electrocoagulation	83.0% after 15 min processing	$[13]$
$Ti4O7$ electrode as anode, current density of 10 mA cm <sup>-2</sup> , initial MO concentration of 150 mg L <sup>-1</sup> , NaCl of 0.01 M	By electrocatalytic oxidation	98.2% after 30 min processing	$[14]$
$\text{Ti/SnO}_2\text{-Sb/PbO}_2\text{-TiO}_2$ nano composite electrode as anode, initial MO concentration of 50 mg $L^{-1}$	By electrocatalytic oxidation	66.4% after 2 h at constant poten- tial	$[27]$
Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>2</sub> /PbO <sub>2</sub> -TiO <sub>2</sub> nanocomposite electrode as anode in 0.1 mol $L^{-1}$ Na <sub>2</sub> SO <sub>4</sub> solution containing 30 mg L <sup>-1</sup> MO with current density of 30 mA cm <sup>-2</sup>	By electrocatalytic oxidation	95.5% after 240 min processing	[28]
Pt electrode as anode for electrocatalysis	By self-powered electrocatalytic oxi- dation	80.0% after 144 h treatment	$[42]$
Pressure of 0.4 MPa, temperature of 35°C, chlorine dioxide concentration of 8 mg L <sup>-1</sup> , pH from 3 to 9	By combining hydrodynamic cavita- tion and chlorine dioxide treatments	90.5% after reaction time of 90 min	$[33]$
SS/PbO <sub>2</sub> -TiO <sub>2</sub> composite electrode as anode, pH6, initial MO concentration of 50 mg L <sup>-1</sup> , current density of 1.75 mA cm <sup>-2</sup>	By electrocatalytic oxidation	99.31% after 50 min processing	Our research

Table 3

Comparison of several results regarding ORP values in the presence of tert-butanol





Fig. 15. Relationship between ORP and *H* (a), ΔORP and *H* (b).

oxidation state of the solution is. The higher the ΔORP value is, the higher the pollutant removal efficiency is. ORP results also can help us predict the oxidation state of ions in solution and whether certain reactions are possible. The results in Table 3 show that all detected ORP values are positive (172.6–452.8 mV), indicating that the solution is capable of oxidizing. Fig. 15 shows that the relationship between ORP and *H* (a), ΔORP and *H* (b) is linear with the same correlation coefficient of 0.9762, nearly independent of the presence of tert-butanol.

# **4. Conclusion**

The  $PbO_2$ -TiO<sub>2</sub> layer can be synthesized directly on the SS substrate by CV method easily, achieving a dense surface and good electrocatalytic ability in MO treatment from solution. MO processing occurs in two stages at different rates, of which the first stage lasted 40 min  $(k = 0.0838 \text{ min}^{-1})$ , which is almost four times faster than the next stage (20 min;  $k = 0.022$  min<sup>-1</sup>). The MO removal efficiency is almost complete after 50 min, reaching 99.31% under optimal processing conditions (current density of  $1.75$  mA cm<sup>-2</sup>, treatment time of 50 min, initial methylene orange concentration of 50 mg  $L^{-1}$  and pH 6). The SS/PbO<sub>2</sub>-TiO<sub>2</sub> stable electrode is an effective anodic material for MO degradation and promising for the electrocatalytic oxidation of other organic pollutants in wastewater. However, the cost of MO processing has not been considered in this study.

## **Abbreviations**



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