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# Optimization of reactive black 5 degradation using hydrothermally synthesized NiO/TiO<sub>2</sub> nanocomposite under natural sunlight irradiation

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# ABSTRACT

In this study, the photocatalytic degradation of reactive black 5 using NiO/TiO<sub>2</sub> nanocomposite as catalyst was optimized based on response surface methodology (RSM). NiO/TiO<sub>2</sub> nanocomposite was fabricated through hydrothermal technique (P = autogenous, T = 150 °C). The nanocomposite fabricated was characterized using powder X-ray diffraction, scanning electron microscopy, UV–vis spectrophotometer, and Fourier transmission infrared spectroscopy. The central composite design (CCD) was applied for the experimental design and process optimization. The optimization studies were carried out by changing initial pH, catalyst dosage, dye concentration, and contact time. The high regression coefficient ( $R^2$  = 0.9460,  $R_{adj}$  = 0.9040) between the variables and the response indicated excellent estimation of experimental data by quadratic model. The optimum catalyst dose, pH, dye concentration, and contact time were found to be 2 g/l, 5, 40 mg/l, and 150 min, respectively, and under the optimal values of process parameters, the dye degradation performance of 86.1% was achieved. Based on the data of present study, it is concluded that CCD and RSM could be employed to model dye degradation parameters using NiO/TiO<sub>2</sub> nanocomposite while optimizing and minimizing the number of experiments required.

Keywords: Optimization; Photocatalysis; Modeling; NiO/TiO<sub>2</sub> nanocomposite; Dye

# 1. Introduction

Currently, environmental pollution has increased more and more public concern. For example, wastewa-

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ter containing dyes resulting from textiles, leather, paper, and plastics industries is generally high in both color and organic content [1,2]. One of the largest class of synthetic dyes used in industries is azo dyes. It has been estimated that approximately 70% of all dyes used in the colored industry are azo dyes [3]. These dyes are

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characterized by the presence of one or more azo bonds (-N=N-) conjugated with aromatic systems, which may also take sulfonic acid groups [4]. Synthetic origin and complex aromatic structure of the dyes make them resistant against microbial biodegradation, therefore, they are not easily degraded through traditional wastewater treatment processes. Hence, their elimination from the effluent is very essential to prevent the entry of colored hazardous materials to nature [5,6]. Some traditional methods such as adsorption [7], nanofiltration membrane [8], electrocoagulation [9], and photodegradation [10,11] have been employed for the treatment of azo dyes containing wastewater. Nevertheless, these methods suffer from some defects such as sludge generation, high treatment costs, adsorbent regeneration, and membrane fouling [3,12]. In the recent years, the application of TiO<sub>2</sub> using solar energy for degradation reactions has attracted the researchers' interest [13]. However, the practical applications of TiO<sub>2</sub>, as a green technology, are limited by the inability to utilize visible light, insufficient quantum efficiency, or the possible photodegradation of the catalyst [14];  $TiO_2$  can only absorb a small portion (3–5%) of solar spectrum in the UV region, resulting in low-photocatalytic efficiency [15,16]. Designing novel catalysts to meet these technical needs is still a challenge [17]. For improving the activity of TiO<sub>2</sub> toward environmental applications, the absorption of light in the visible light spectrum must be enhanced [18]. Therefore, many methods have been used to improve photocatalytic efficiency of TiO<sub>2</sub>-based photocatalysts into the visible light region, including doping TiO<sub>2</sub> materials with other impurities such as metals or non-metal elements, photosensitization, and composite semiconductors [19,20]. Moreover, conventional designing experiments are time consuming and require more energy to obtain photodegradation results. Response surface methodology (RSM) is a powerful experiment design tool used widely to design, optimize, and evaluate the performance of multivariable systems. In addition, it gives a complete interaction effects of all of the parameters influencing the process [21,22]. The main advantages of RSM lie in the fact that this method builds models quickly, is less time consuming than the classical methods, cost-effective, and more accurate in an optimization design [23,24].

Thus, the aim of this study was to synthesize NiO/ $TiO_2$  nanocomposite and to investigate the photocatalytic degradation of reactive black 5 (RB5), a model azo dye, in the presence of natural sunlight. NiO/TiO<sub>2</sub> nanocomposite was synthesized via hydrothermal method and RSM was used for the experimental design and optimization of RB5 degradation.

# 2. Materials and methods

## 2.1. Materials

Reagent grade TiO<sub>2</sub>, NiO, triethylamine and HCl were purchased from Merck, Germany. Water typeone and double distilled water were produced by a TKA Smart 2 ultrapure water production system (Thermo Electron LED GmbH, Germany). RB5 (Alvan Sabet Co., Iran) was used as a model pollutant from textile industry. Table 1 shows the chemical structure and some characteristics of this dye.

# 2.2. Experimental

NiO/TiO<sub>2</sub> nanocomposite was fabricated under mild hydrothermal conditions ( $T = 150^{\circ}$ C, P = autogenous, t = 12 h). Three moles of ZnO, 1 mol of nickel oxide, and 10 ml of 1 mol HCl were added into a Teflon liner ( $V_{\text{fill}} = 10 \text{ mL}$ ). At the same time, a fixed volume (1 ml) of triethylamine was added to the above-mentioned mixture and it was stirred vigorously for a few minutes. Later, the Teflon liner was placed inside a General Purpose autoclave. Then, the assembled autoclave was kept in an oven with a temperature programmer-controller for 12 h. The temperature was kept at 150°C. After the experimental run, the autoclave was quenched to the room temperature. The product in the Teflon liner was then transferred to a clean beaker, washed with double distilled water several times, and then allowed to settle down. The surplus solution was removed using a syringe. Then, the remnant was allowed to dry naturally at room temperature. The dried particles were subjected to systematic characterization and photocatalytic studies.

## 3. Results and discussion

#### 3.1. Characterization of NiO/TiO<sub>2</sub> nanocomposites

## 3.1.1. Powder XRD

The crystal structure of NiO/TiO<sub>2</sub> nanocomposite was evaluated using Powder X-ray diffraction (XRD). The XRD plot was taken in the angular range of  $2\theta = 5^{\circ}-110^{\circ}$ . The XRD plot of NiO/TiO<sub>2</sub> was checked and assessed with reagent grade TiO<sub>2</sub> and NiO using Match software (CRYSTAL IMPACT, Germany). As Fig. 1 indicates, mixed phases of NiO and TiO<sub>2</sub> were observed in the XRD pattern. However, the dominated phase is TiO<sub>2</sub> (anatase phase). Moreover, the peaks of crystal were slightly displaced, which could be attributed to the effect of NiO on the TiO<sub>2</sub> lattice.

# Table 1 The chemical properties of RB5



Fig. 1. Powder XRD plot of NiO/TiO<sub>2</sub> nanocomposite.

# 3.1.2. Scanning electron microscopy

The morphology of NiO/TiO<sub>2</sub> nanocomposite was investigated using Scanning Electron Microscopy (SEM) (Fig. 2). It is evident that the nanocomposite has a spherical structure with no agglomeration, which could be contributed to the effect of surface modifier applied [25]. Moreover, most of the particles

are homogeneous, having uniform structure with different size distribution.

# 3.1.3. FT-IR analysis

Fig. 3 shows the FT-IR spectrum of  $NiO/TiO_2$  nanocomposite. In order to assign the FT-IR spectrum,

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Fig. 2. SEM image of NiO/TiO<sub>2</sub> nanocomposite.



Fig. 3. FT-IR Spectrum of NiO/TiO<sub>2</sub> nanocomposite.

the absorption peaks were compared with the standard pattern [26]. The spectrum was recorded in the wavelength range 400–4,000 cm<sup>-1</sup>. The peaks around 400– 500, 750, and 850 cm<sup>-1</sup> are attributed to the Ti–O bond in the TiO<sub>2</sub> lattice, the Ni–O bond stretching, and N–H group in surface modifier, respectively. The sharp peak with medium intensity at 1,200 cm<sup>-1</sup> is assigned to the C–N group. The bands at 1,600 and 2,900 cm<sup>-1</sup> correspond to N–H and C–H bond stretching, respectively. In addition, the broadband at 3,400 cm<sup>-1</sup> was observed. It indicates the presence of OH groups absorbed by the sample from the atmosphere.

## 3.1.4. Bandgap energy of NiO/TiO<sub>2</sub> nanocomposite

One of the drawbacks of using  $TiO_2$  in photocatalytic applications lies in its large bandgap,  $E_{g}$ , which limits the spectrum of photons that can create electron–hole pairs to participate in oxidation or reduction reactions to the UV and corresponds to only 4% of the incident solar energy [27]. The  $E_g$  of NiO and TiO<sub>2</sub> are 3.86 and 3.20 eV, respectively [28]. UV–vis spectrophotometer was used for determining the effect of adding NiO on the optical properties of TiO<sub>2</sub>. As Fig. 4 indicates, the absorption edge of NiO/TiO<sub>2</sub> nanocomposite was decreased. This red shift can be attributed to the charge transfer transitions between the metal ion *d* electrons and the conduction or valence band of TiO<sub>2</sub> [29].

# 3.2. Photocatalytic degradation of RB5

The dye degradation experiments were carried out by mixing different amounts of NiO/TiO<sub>2</sub> nanocomposite (0.5-2.5 g/l) for RB5 in a beaker containing 200 ml of a dye solution (40-800 mg/l) and at various pH (3-11). Before exposing the sample into the sunlight illumination, the solution was kept in darkness under continuous shaking for 30 min in order to reach adsorption/desorption equilibrium. However, no adsorption was observed after keeping the solution in darkness. The initial pH of the solution was adjusted before the experiment using 0.1 N NH<sub>3</sub>OH or HCl and was controlled using pH meter. Then, solution was irradiated under natural sunlight. The period of the experiment was between 11:30 and 14:30 during the month of June. At specific time intervals, 5 ml of the dye sample was taken out from the system. Each sample was centrifuged for 5 min at 5,000 rpm. The maximum wavelength ( $\lambda_{max}$ ) used for the determination of residual concentration of RB5 in the solution



Fig. 4. Bandgap energy of NiO/TiO<sub>2</sub> nanocomposite.

was 618 nm using UV–vis spectrophotometer. The degradation efficiency (R%) was calculated using the following equation:

Degradation efficiency 
$$(R\%) = (A_0 - A)/A_0 \times 100$$
 (1)

where  $A_0$  and A are the dye concentration (mg/l) at time 0 and t respectively in Eq. (1).

## 3.3. Experimental design and data analysis

In the present study, central composite design (CCD) optimized the degradation of RB5 in the presence of natural sunlight using NiO/TiO<sub>2</sub>. The statistical software "Design Expert" (Version 8) was applied for CCD. Independent variables for this investigation were catalyst dosage, pH, contact time, and dye concentration. As a result, the CCD matrices of 31 experiments were designed at 5 levels consisting of 16 factorial points, 8 axial points ( $\alpha = 2$ ), and 7 replicates at the center point (Table 2).

The treatment of the dye degradation process is explained by an empirical quadratic model. A quadratic model, which also includes the linear model, is given as:

$$\eta = b_0 + \sum_{i=1}^n b_i x_i + \sum_{i=1}^n b_{ii} x_i^2 + \sum_{i=1}^{n-1} \sum_{i=1}^n b_{ij} x_i x_j$$
(2)

where  $\eta$  is the dye removal performance,  $b_0$  the constant coefficient,  $b_i$  the linear coefficient,  $b_{ii}$  the quadratic coefficient,  $b_{ij}$  the interaction coefficient, and  $x_i$  and  $x_i$  are the coded values of the variables [5].

### 3.4. Modeling and optimization of RB5 photodegradation

The experimental results of dye degradation by nanocomposite synthesized were analyzed through RSM to obtain an empirical model. Based on these results, an empirical relationship between the responses and independent variables was achieved for dye degradation expressed by quadratic polynomial equation (Eq. (3)):

$$R = (-181.66) + (20.52 X_1) + (68.61 X_2) + (0.9973 X_3) + (4.327 X_4) + (-1.318 X_1 X_2) + (-7.08 X_1 X_3) + (-0.101 X_1 X_4) + (0.0175 X_2 X_3) + (-8.21 X_1 X_4) + (-1.6297 X_1^2) + (-15 X_2^2) + (-3.688 X_3^2) + (-0.048504 X_4^2)$$
(3)

In Eq. (3), R is the response degradation percent,  $X_1$ ,  $X_2$ ,  $X_3$ , and  $X_4$  are corresponding to independent variables of pH, catalyst dosage (g/l), contact time (min), and dye concentration (mg/l) respectively.

Table 3 presents the results of ANOVA analysis of the quadratic models. ANOVA checks adequacy of the developed model and statistical significance of the regression coefficients [30].

Moreover, in Table 3, the quadratic model F-value of 37.97 implies that the model is significant for the degradation of RB5 and there is only a 0.01% chance that a "model F-value"; this large could occur due to noise. Adequate precision measures the signal to noise ratio and a ratio greater than 4 is generally desirable [3,31]. Therefore, in the guadratic model of RB5 degradation, the ratio of 23.53 indicated an adequate signal. The square of correlation coefficient for responses was computed as the  $R^2$ . The goodness of fit of the model was also checked by the multiple correlation coefficient. The  $R^2$  value of 0.9460 for degradation of RB5 using NiO/TiO<sub>2</sub> nanocomposite and corresponding adjusted  $R^2$  0.9040 are close to 1.0 indicating a high correlation between the observed values and the predicted values [12]. Table 4 presents the optimum conditions for maximum efficiency of dye photodegradation.

Fig. 5 shows the relationship between the actual and the predicted values for the degradation of RB5 using NiO/TiO<sub>2</sub> nanocomposite. Actual values and perfected values were measured from the response data for a particular run and the model, respectively. The results showed that the predicated values and the actual values obtained for dye degradation were high. In addition, it was found that the models developed were effectual in taking correlation between nanocomposite type variables and degradation of dye [32,33].

Table 2

Experimental design of photocatalytic degradation of RB5 dye using NiO/TiO2 nanocomposite

Factor	Name	Low actual	Height actual
$\overline{X_1}$	pН	3	11
X <sub>2</sub>	Catalyst dosage (g/l)	0.5	2.5
$X_3$	Contact time (min)	60	180
X <sub>4</sub>	Dye concentration (mg/l)	40	80

Source	Sum of square	DF	Mean square	<i>F</i> -value	<i>p</i> -value	
Model	12,138.79	14	867.04	37.97	< 0.0001	
$X_1$	987.44	1	987.44	43.24	< 0.0001	
X <sub>2</sub>	65.95	1	65.95	2.89	< 0.0001	
X <sub>3</sub>	26.21	1	26.21	1.15	0.2999	
$X_4$	835.32	1	835.32	36.58	< 0.0001	
$X_1X_2$	27.83	1	27.83	1.22	0.2860	
$X_1X_3$	2.89	1	2.89	0.13	0.7267	
$X_1X_4$	65.61	1	65.61	2.87	0.1065	
$X_2X_3$	1.10	1	1.10	0.048	0.8289	
$X_2X_4$	0.12	1	0.12	5.39	0.9425	
$X_3X_4$	0.950	1	0.95	0.042	0.8454	
$X_{1}^{2}$	1,215.31	1	1,215.31	53.21	< 0.00001	
$X_2^2$	450.51	1	450.51	19.73	0.0042	
$X_{3}^{\bar{2}}$	247.45	1	247.45	10.48	0.0046	
$X_4^2$	672.76	1	672.76	29.46	< 0.0001	
Residual	345.60	16	22.48	-	_	
Lack of fit	365.08	10	36.51	695.39	< 0.0001	
Total	12,504	30	-	-	-	

Table 3 ANOVA result of the quadratic model of photocatalytic degradation of RB5 dye using NiO/TiO<sub>2</sub> nanocomposite

Notes:  $X_1 = pH$ ,  $X_2 = catalyst$  dosage,  $X_3 = contact$  time,  $X_4 = dye$  concentration,  $R^2 = 0.9460$ ,  $R^2$ -(adj) = 0.9040.

Table 4 Optimum values of the process parameter for maximum efficiency

Parameter	Optimum value BR5		
$\eta$ (efficiency, %)	0.861		
X <sub>1</sub> (pH)	5		
$X_2$ (catalyst dosage, g/l)	2		
$X_3$ (contact time, min)	150		
$X_4$ (concentration dye, mg/l)	40		

A suitable graphical method for judging and explaining the systematic departures from the assumption that errors are normally distributed and are independent of each other is the normal probability plot of the residuals. Plot of residual vs. the predicted response is presented in Fig. 6. Based on this plot, the residuals appear to be randomly scattered and all the residual values are within the range of -3 and +3 (values between -3 and +3 being the acceptable limit), thereby validating the model [34,35].

The effect of operating parameters of pH, catalyst dosage, initial dye concentration, and contact time on dye degradation are shown in the response surface graphs in Figs. 6–8. As shown in Fig. 6, degradation efficiency (%) of RB5 dye decreased with an increase in initial solution pH and the maximum degradation efficiency was observed at pH 5.0. This can be explained based on zero point of charge (pH<sub>zpc</sub>) of

TiO<sub>2</sub>. The point of  $pH_{zpc}$  for TiO<sub>2</sub> nanoparticles is about 6.5 [36]. In acidic solution, TiO<sub>2</sub> surface is positively charged, while it is negatively charged in alkaline solution. RB5 is an anionic dye, which after ionization at acidic pH, has a tendency to be adsorbed onto the TiO<sub>2</sub> surface. As a result, positively charged surface of TiO<sub>2</sub> enhanced the adsorption of RB5 by the electrostatic attraction, which would increase the degradation of RB5. But, in alkaline medium, the surface of TiO<sub>2</sub> has become negatively charged that leads to the electrostatic repulsion between RB5 and nanocomposite, which results in decreasing the degradation efficiency [4,37].

Fig. 7 represents the effects of catalyst dosage and contact time on the degradation of RB5 by NiO/TiO<sub>2</sub> nanocomposite at an initial dye concentration of 30 mg/l and pH of 5. As depicted in Fig. 6, the degradation efficiency increased as the NiO/TiO<sub>2</sub> nanocomposite ratio increased from 0.5 to 2 g/l and then decreased as the ratio increased from 2 to the highest value of 2.5. This can be explained on the basis that the increase in catalyst loading is accompanied by an increase in the number of active sites on the NiO/ TiO<sub>2</sub> surface, which increase the number of hydroxyl and superoxide radicals. However, when the catalyst loading exceeded the limiting value, due to decrease in sunlight penetration into the solution, causes a decrease in the RB5 degradation rate. Moreover, at high photocatalyst dosage the photocatalyst surface reduced due to the agglomeration [38,39].



Fig. 5. Plot of the predicted vs. the experimental degradation efficiency.



Fig. 6. Plot of the normal probability of the raw residuals.



Fig. 7. The response surface plot and corresponding counter plot of RB5 as the function of initial pH and reaction time (min). NiO/TiO<sub>2</sub> = 1.5 g/l, initial dye concentration = 40 mg/l.



Fig. 8. The response surface plot and counter plot of RB5 as the function of initial catalyst dosage (g/l), contact time (min), Initial pH 5, and initial dye concentration = 40 (mg/l).

The effect of the initial dye concentration on the degradation efficiency is shown in Fig. 9 at a nanocomposite ratio of 1.5 and initial pH of 5. Fig. 9

shows that increasing initial dye concentration from 40 to 80 mg/l results in decreasing degradation efficiency. At high dye concentrations, the formation



Fig. 9. The response surface plot and counter plot of RB5 degradation as the function of initial dye concentration, pH, initial catalyst dosage = 1.5 g/l, and reaction time = 150 min.

reactive oxygen species on the photocatalyst surface is reduced. In addition, as the concentration of solution increases the path length of photon entering into the dye solution decreased, thus, only fewer photons reached the catalyst surface. Hence, the absorption of photons by the catalyst decreases, and consequently, the degradation efficiency decreases [40,41].

# 4. Conclusion

In this investigation, the photocatalytic degradation of a simulated dyestuff effluent, containing RB5 as colorant, was studied and the effects of the operating variables including initial dye concentration, NiO/ TiO<sub>2</sub> dosage, pH, and time on degradation efficiency were investigated using RSM method. Results of ANOVA analysis indicated a high coefficient of determination value ( $R^2 = 0.9460$ ,  $R_{adi} = 0.9040$ ), therefore ensuring a satisfactory adjustment of the quadratic model with the experimental data. In addition, an optimum condition for the degradation process using RSM was achieved at dye concentration of 40 mg/l, initial pH value of 5, catalyst dosage 2 g/l, and contact time of 150 min for RB5. Based on the results obtained, it is concluded that the RSM is one of the suitable methods to optimize the best operating conditions to maximize the dye removal.

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