



## Adsorption of Ni(II) using amine-functionalized MCM-41 optimized by response surface methodology

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### ABSTRACT

Adsorption of Ni(II) by amine-functionalized MCM-41 (NH<sub>2</sub>-MCM-41) was studied with response surface methodology (RSM) employed to optimize the adsorption process. The independent variables include pH, metal concentration, temperature, and adsorbent dosage. Analysis of variance (ANOVA) of RSM indicated that the obtained second-order polynomial model was appropriate to predict the adsorption process. Meanwhile, the maximum removal efficiency for Ni(II) was 93.20%, which was achieved at pH 6.50, metal concentration 10.00 mg/L, temperature 35°C, and adsorbent dosage 5.00 g/L. The kinetic study revealed that the pseudo-second-order kinetic model could describe the experimental data better. While the intraparticle diffusion model suggested three stages of the adsorption process. In addition, the adsorption data conformed well to Langmuir isotherm model. Thermodynamic study implied the adsorption process was spontaneous and endothermic. The adsorption-desorption experiment showed that NH<sub>2</sub>-MCM-41 held good reusability.

*Keywords:* Ni(II); NH<sub>2</sub>-MCM-41; Response surface methodology; Kinetic; Isotherm

### 1. Introduction

The immoderate discharge of wastewater-containing heavy metals can pollute the surface and ground water, which may threaten the fresh water sources, and then be hazardous to animals and human beings. Among the various heavy metal ions, nickel is known as one of the toxic elements. Excess uptake of nickel (estimated as 0.05 mg/cm<sup>3</sup> in nickel per 40 h work [1]) may directly or indirectly cause health effects on human beings, for example, diarrhoea,

nephritic syndrome, serious lung and kidney problems, pulmonary fibrosis, and skin dermatitis [2]. In view of this, the World Health Organization has set the permissible limit of 0.02 mg/L for nickel in drinking water. However, wastewater discharge from industries, such as batteries manufacturing, mine, electronic, electroplating, and metal cleaning [3] often contains high concentrations of nickel that may cause serious problems. Thus, it is essential to removal nickel from wastewater before its emission.

As one of the most effective and attractive method, adsorption, with the advantages of no chemical sludge and high removal efficiency [4,5], has been widely

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used in the removal of heavy metal ion from aqueous solution. Furthermore, researcher has made enormous effort in the exploitation of new, cheaper, and effective adsorbents for heavy metal removal in the recent years. The tested adsorbents include zeolites [6], natural kaolinite [7], activated carbon prepared from apricot stone [8], tea factory waste [9], rice bran [10], and so on. In the family of mesoporous materials, MCM-41 plays a significant role. It owns large pore volume, high surface area, regular channel, and good thermostability [11,12], which made it a potential adsorbent. Hokura et al. [13] reported the adsorption of Cu(II) by MCM-41 and they found it effective as an adsorbent; Parida and Dash [14] reported that adsorption capacity of Fe-MCM-41 toward Cu(II) reached maximum at pH 5.5, temperature 323 K, and Cu(II) concentration of 59.6 mg/L; Qin et al. [15] demonstrated ammonium-functionalized MCM-41 was effective in absorbing four kinds of anionic dyes. Moreover, MCM-41 was usually modified to achieve better adsorption results.

Response surface methodology (RSM) is one of the most popularly used methods in research on sorption [16]. It combines mathematical and statistical techniques to evaluate the relative significance of process parameters in the presence of complex interactions [17], as well as to capture the nonlinear relationships between independent parameters and system response.

In the present work, amine-functionalized MCM-41 was synthesized and used as an adsorbent in the removal of Ni(II) from solution. Moreover, RSM was employed to optimize the adsorption process with variables such as pH, metal concentration, temperature, and adsorbent dosage studied. Adsorption isotherms were applied to describe the equilibrium data. Kinetics and thermodynamics were also studied for better evaluating the adsorption mechanism. At last, regeneration of the adsorbent was tested as well. The aim of this paper is to show the availability of NH<sub>2</sub>-MCM-41 to adsorb Ni(II) from solution.

## 2. Materials and methods

### 2.1. Materials

A stock solution of Ni(II) (1,000 mg/L) was prepared in the way as follows: 0.1000 g Ni (99.9%) dissolved in 10 mL of (1 + 1) Nitric Acid, then the solution was heated to nearly dry, followed by dissolving the solid in 1% Nitric Acid, and then diluted with distilled water to 1,000 mL. The stock solution was diluted with distilled water to obtain desired concentration in experiments.

### 2.2. Characterization of the adsorbent

The pristine MCM-41 was purchased (Tianjin kay, science and technology development co., Ltd., China) and NH<sub>2</sub>-MCM-41 was synthesized according to the method in our previous work [18]. All other chemicals used were of analytical grade and used without further purification. Nitrogen adsorption-desorption isotherms were determined by an ASAP 2010. X-ray diffraction (XRD) of the adsorbent was measured with an X-ray diffractometer (ARL Corporation, Switzerland) using Ni filter CuK $\alpha$  at 40 kV and 30 mA over the range of 1°–8°. Besides, in order to analyze the chemical properties of NH<sub>2</sub>-MCM-41 before and after adsorption, Fourier transform infrared (FTIR) spectra was obtained using a Bruker corporation instrument (German) with all spectra recorded at 4,000–750 cm<sup>-1</sup> wavenumber. Moreover, microscopic appearance of the adsorbent was studied by field emission scanning electron microscope (SEM) (S4800, Carl Zeiss AG, Germany) with the images taken at 5.0 kV. X-ray Fluorescence (XRF) (ThermoFisher Scientific Corporation) was used to analyze the adsorbent chemical composites.

The pH in the point of zero charge (pH<sub>pzc</sub>) for NH<sub>2</sub>-MCM-41 was determined as follows [19]: 25 mL of 0.01 M NaCl were added to a series of 250 mL conical flasks, and the initial pH was adjusted between 2 and 12 using 0.1 M NaOH or 0.1 M HCl. Then, 0.08 g of NH<sub>2</sub>-MCM-41 was added to each flask with the final pH measured after agitation for 48 h. Afterward, difference between the initial pH and final pH (initial pH–final pH) was plotted against the initial pH. The point, at which the resulting curve intersected with abscissa, gave the pH<sub>pzc</sub>.

### 2.3. Adsorption studies

Batch adsorption experiments were conducted according to the RSM design. The experiments were carried out in conical flasks of 250 mL containing 100 mL nickel solution at a known concentration. pH of the solution was adjusted with 0.1 M HCl or NaOH. Then, the conical flasks were placed in a shaker at 130 rpm for 180 min. After adsorption, the samples were separated by centrifugation at 8,000 rpm, and the supernatant was used to determine the residual nickel concentration with a UV-spectrophotometer (Ruili Analytical Instrument Corporation Ltd., Beijing, China) at 530 nm. In addition, the comparison experiment was conducted with 0.1 g MCM-41 and NH<sub>2</sub>-MCM-41 respective with 100 mL of metal solution (10 mg/L) at pH 6.0. For isotherm study, experiments

were carried out with 0.35 g adsorbent, metal concentration in the range of 10–50 mg/L, at pH 6.5, and temperature 25, 30, and 40 °C, respectively. For kinetic study, experiments were performed with 0.35 g of NH<sub>2</sub>-MCM-41, 100 mL of nickel solution (30 mg/L) at 30 °C, and pH 6.5. And the supernatant was withdrawn at 15, 30, 60, 90, 120, 150, and 180 min, separately. The Removal (%) and adsorption capacity  $q_e$  (mg/g) were calculated by the equations following:

$$\text{Removal} = \frac{C_0 - C_e}{C_0} \times 100\% \quad (1)$$

$$q_e = \frac{(C_0 - C_e)V}{M} \quad (2)$$

where  $C_0$  is the initial Ni(II) concentration (mg/L),  $C_e$  is the final Ni(II) concentration (mg/L),  $V$ (mL) is the volume of solution, and  $M$ (g) is the mass of dry adsorbent. All these experiments were conducted in triplicate.

#### 2.4. Desorption study

After adsorption process, the adsorbent was recovered by mixing metal-loaded adsorbent with 25 mL of 1 M HNO<sub>3</sub>, and agitated at the speed of 130 rpm for 180 min.

#### 2.5. Experimental design

The Design Expert software (Stat-Ease, Inc., Minneapolis, USA) was used for regression and graphical analysis of the experimental data.

The optimum conditions for the adsorption of Ni(II) by NH<sub>2</sub>-MCM-41 was determined based on a central composite design (CCD) under RSM. And the optimum studies were carried out with four response variables: pH ( $X_1$ ), metal concentration ( $X_2$ ), temperature ( $X_3$ ), and adsorbent dosage ( $X_4$ ). For statistical calculation, the variables  $X_i$  were coded as  $Z_i$  according to the following equation:

$$Z_i = \frac{X_i - X_0}{\Delta X} \quad (3)$$

where  $Z_i$  is a coded value of the variable,  $X_i$  is actual value of variable,  $X_0$  is value of the  $X_i$  at the center point, and  $\Delta X$  the step change value. The actual value and coded value of the variables are shown in Table 1. To explain relationship between the independent variables and the response, a quadratic equation was used:

$$R (\%) = a_0 + \sum_{i=1}^n a_i X_i + \sum_{i=1}^n a_{ii} X_i^2 + \sum_{i=1}^{n-1} \sum_{j=2}^n a_{ij} X_i X_j + e \quad (4)$$

where  $a_0$  is the constant coefficient,  $a_i$ ,  $a_{ii}$ , and  $a_{ij}$  are the regression coefficients,  $X_i$  and  $X_j$  indicate the independent variables in the form of coded values, and  $e$  is the random error.

### 3. Results and discussion

#### 3.1. Characterization of the adsorbent

The BET surface area, total pore volume, and mean pore radius of NH<sub>2</sub>-MCM-41 were 658 m<sup>2</sup>/g, 0.78 cm<sup>3</sup>/g, and 2.74 nm, respectively, while that of MCM-41 were 821 m<sup>2</sup>/g, 0.94 cm<sup>3</sup>/g, and 3.02 nm, respectively. There existed significant decrease in the surface area, total pore volume, and mean pore radius of NH<sub>2</sub>-MCM-41 when compared with MCM-41. This may result from the amine groups in the framework channels [20] and adsorbent surface.

The XRD spectra of MCM-41, NH<sub>2</sub>-MCM-41, NH<sub>2</sub>-MCM-41-Ni, and Ni-desorbed NH<sub>2</sub>-MCM-41 in the range of 1°–8° were illustrated in Fig. 1. As shown in Fig. 1, all spectra owned a diffraction peak in the range of 1°–3°, even though the intensity of the peak decreased, corresponding to the (100) plane of hexagonal cell of MCM-41. The intensity decrease of the (100) plane and the disappearance of the (110) plane may due to the graft of amine. Thus, it can be confirmed that the hexagonal structure of MCM-41 was preserved after modified by amine group. In addition, the XRD patterns of NH<sub>2</sub>-MCM-41 before and after the regeneration had the similar trend, demonstrating that the effect of adsorbent regeneration process on the structure of NH<sub>2</sub>-MCM-41 was weak.

FTIR spectrum of NH<sub>2</sub>-MCM-41 before and after adsorption of Ni(II) are shown in Fig. 2. The FTIR analysis had shown that amino was successfully grafted on MCM-41 in our previous work [18]. Upon Ni(II) loading, the peak intensity of NH<sub>2</sub>-MCM-41 at 1,541.1/cm (bending vibration of N–H group) was weakened, this may be attributed to the presence of a lesser number of functional groups on NH<sub>2</sub>-MCM-41 [21]. Moreover, the peak at 1,541.1/cm exhibited band shift. Thus, we speculated it was caused by the adsorption of Ni(II), and the amine group may be involved in the adsorption process. This point was also reported by other researchers (Malkoc and Nuhoglu [3], Sheng et al. [22]). Besides, Sun et al. [23] studied the adsorption of heavy metal

Table 1  
The independent variables and their levels in the experiment design

Factors		Coded values				
		$-\alpha$ (-2)	-1	0	1	$\alpha$ (2)
pH	$X_1$	0.5	2.5	5	7.5	10
Metal concentration (mg/L)	$X_2$	0	10	30	50	70
Temperature (°C)	$X_3$	10	20	30	40	50
Adsorbent dosage (g/L)	$X_4$	0	1	3	5	7

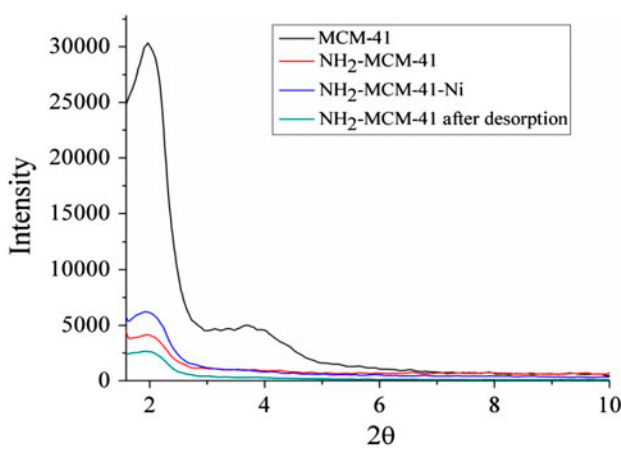


Fig. 1. Small angle XRD spectra of MCM-41,  $\text{NH}_2$ -MCM-41,  $\text{NH}_2$ -MCM-41-Ni, and desorbed  $\text{NH}_2$ -MCM-41.

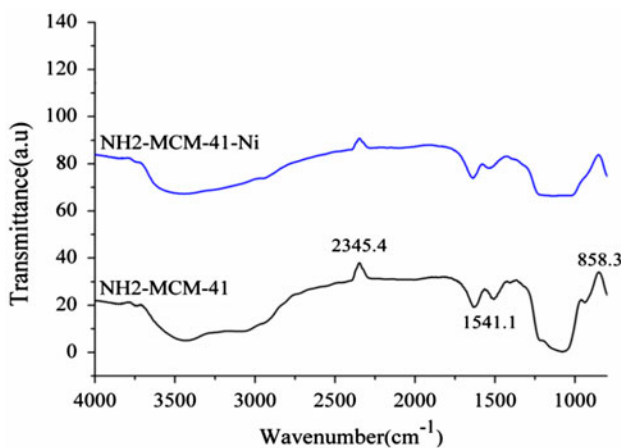


Fig. 2. FTIR spectra of  $\text{NH}_2$ -MCM-41 and  $\text{NH}_2$ -MCM-41-Ni.

ions on chitosan/cellulose composite biosorbent. The  $1,599/\text{cm}$  ( $-\text{NH}$  bending vibration) was weakened after adsorption and they inferred that the amine group was

involved in the adsorption process. Moreover,  $\text{Ni(II)-N}$  coordinate bonds were claimed to be formed. Boddu et al. [21] reported the removal of arsenic(III) and (V) using chitosan-coated biosorbent. In their study, the intensity of transmittance of peaks ( $-\text{NH}$  vibration) was relatively more in case of metal ions-loaded adsorbent, and they attributed this to the lesser number of functional groups (including  $-\text{NH}_2$ ) that involved in binding the metal ions.

The FE-SEM images of MCM-41,  $\text{NH}_2$ -MCM-41, and Ni-loaded  $\text{NH}_2$ -MCM-41 were provided as shown in Fig. 3. Compared with MCM-41, the image of  $\text{NH}_2$ -MCM-41 showed that the graft of amine groups on MCM-41 did not bring about significant change to the mesoporous structure of MCM-41. While some of the pore may be blocked. Whereas, a large number of tiny particles emerged on the surface of  $\text{NH}_2$ -MCM-41 after Ni(II) adsorption process as illustrated in Fig. 3(c); it may imply that Ni(II) could be successfully adsorbed on  $\text{NH}_2$ -MCM-41.

### 3.2. Comparison removal efficiency

A comparison for the removal efficiency of Ni(II) by  $\text{NH}_2$ -MCM-41 and MCM-41 was made, as shown in Fig. 4. It can be seen from Fig. 4 that the Ni(II) removal efficiency were, respectively, 70.51 and 39.42% for  $\text{NH}_2$ -MCM-41 and MCM-41. The grafted of amidogen on MCM-41 had greatly improved the adsorption capacity of MCM-41 for Ni(II). Therefore,  $\text{NH}_2$ -MCM-41 owned the potential to be used in the removal of Ni(II).

### 3.3. Fitting of the process model and statistical analysis

In the optimization experiment, a total of 30 runs of CCD-designed experiments were conducted and the results are presented in Table 2. Through multiple regression analysis on the experiment data, the predicted model, a second-order polynomial function, was achieved:

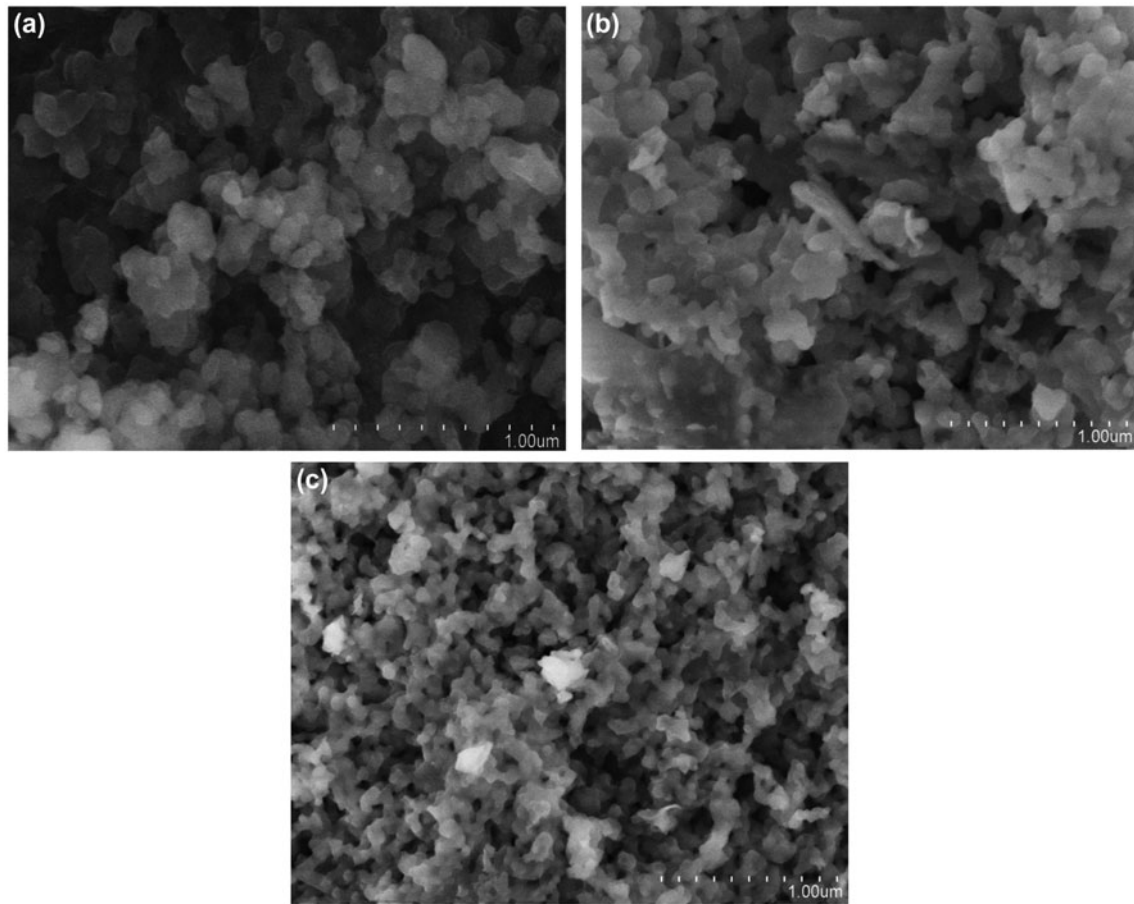


Fig. 3. SEM images of MCM-41 (a), NH<sub>2</sub>-MCM-41 (b), and Ni-loaded NH<sub>2</sub>-MCM-41 (c).

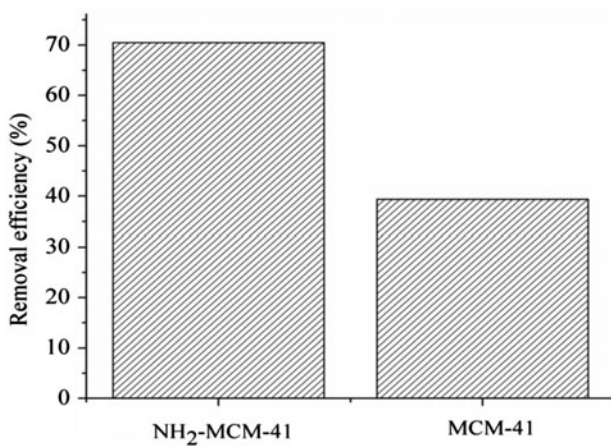


Fig. 4. Comparison removal efficiency of NH<sub>2</sub>-MCM-41 and MCM-41 for Ni(II).

$$\begin{aligned}
 Y_{\text{Ni(II)}} = & 48.50 + 15.22X_1 - 12.45X_2 + 8.50X_3 + 10.76X_4 \\
 & + 4.16X_1^2 + 6.49X_2^2 - 3.86X_3^2 - 4.26X_4^2 \\
 & - 1.81X_1X_3 + 2.72X_1X_4 + 3.04X_2X_3
 \end{aligned} \quad (5)$$

In this equation, the positive values indicated that these terms increase the response, while the negative values decrease the response [24]. The results of Analysis of variance (ANOVA) for the predicted model and each variable are given in Table 3. In Table 3, the large model *F* value (73.35) and low probability “*p*” value (<0.0001) indicated high significance of the predicted model. It implied that the model can explain relation between the response and variables appropriately. Moreover, applicability of the model can be checked by the determined coefficient (*R*<sup>2</sup>) and adjusted *R*<sub>adj</sub><sup>2</sup> [25] as well. The value of *R*<sup>2</sup> (0.9856) and adjusted *R*<sub>adj</sub><sup>2</sup> (0.9722) were all close to 1, which demonstrated applicability of the model as well as a high correlation between the actual and predicted values.

Table 2  
Experiment design and results of the CCD

Run order	Coded values				Response (%)	
	$X_1$	$X_2$	$X_3$	$X_4$	Observed value	Predicted value
1	-1	-1	-1	-1	37.50	35.73
2	+1	-1	-1	-1	63.50	62.68
3	-1	1	-1	-1	6.80	1.26
4	1	1	-1	-1	31.20	29.88
5	-1	-1	1	-1	52.50	49.45
6	1	-1	1	-1	70.70	69.17
7	-1	1	1	-1	29.20	27.15
8	1	1	1	-1	50.80	48.55
9	-1	-1	-1	1	48.90	47.76
10	1	-1	-1	1	85.10	86.22
11	-1	1	-1	1	18.60	19.20
12	1	1	-1	1	58.40	58.70
13	-1	-1	1	1	63.30	63.38
14	1	-1	1	1	91.50	94.28
15	-1	1	1	1	48.60	46.66
16	1	1	1	1	78.10	78.93
17	-2	0	0	0	32.50	37.59
18	2	0	0	0	98.20	96.80
19	0	-2	0	0	99.10	98.95
20	0	2	0	0	45.30	49.14
21	0	0	-2	0	13.60	15.72
22	0	0	2	0	48.10	49.67
23	0	0	0	-2	2.20	9.52
24	0	0	0	2	56.20	52.57
25	0	0	0	0	48.40	48.38
26	0	0	0	0	48.50	48.38
27	0	0	0	0	48.10	48.38
28	0	0	0	0	48.30	48.38
29	0	0	0	0	48.60	48.38
30	0	0	0	0	48.40	48.38

Besides, the predicted vs. actual removal efficiency for Ni(II) are illustrated in Fig. 5, where the predicted values were calculated according to Eq. (5) and the actual values were measured data for each run in the CCD design. It can be detected from Fig. 5 that the predicted and actual values were in good agreement.

### 3.4. Effect of process variables

Sensitivity of the response to two interactive variables can be displayed by holding the other variables at central values. Based on the ANOVA results, the pH with a  $F$ -value of 334.23 and “ $p$ ” value less than 0.0001 was found to have the greatest effect on the removal of Ni(II) by  $\text{NH}_2\text{-MCM-41}$ . The other three variables also exhibited significant effect on Ni(II) removal in the order of metal concentration

( $F = 223.77$ ,  $p < 0.0001$ ) > adsorbent dosage ( $F = 167.11$ ,  $p < 0.0001$ ) > temperature ( $F = 104.13$ ,  $p < 0.0001$ ). The effect of the four process variables on the response are shown in the 3D response surface plots (Figs. 6(a)–(c) and 7(a)–(c)).

#### 3.4.1. Effect of pH

The combined effects of pH with metal concentration, temperature, and adsorbent dosage are shown in Fig. 6(a)–(c). As can be seen from Fig. 6(a)–(c), the removal efficiency of Ni(II) increased with increase pH ranging from 2.5 to 6.5. This phenomenon can be explained by the different dominant form of Ni(II). It is clear that Ni(II) presents in the forms of  $\text{Ni}^{2+}$ ,  $\text{Ni}(\text{OH})^+$ ,  $\text{Ni}(\text{OH})_2^0$ , and  $\text{Ni}(\text{OH})_3^-$  at different pH values (Fig. 8(a)). At  $\text{pH} < 8.0$ , the main species is  $\text{Ni}^{2+}$ .

Table 3  
ANOVA for the fitted quadratic polynomial model for Ni(II) adsorption

Source	Sum of squares	df	Mean square	F-value	Prob > F
Model	16,935.24	14	1,209.66	96.58	<0.0001
$X_1$	5,259.92	1	5,259.92	419.94	<0.0001
$X_2$	3,722.55	1	3,722.55	297.20	<0.0001
$X_3$	1,728.90	1	1,728.90	138.03	<0.0001
$X_4$	2,779.95	1	2,779.95	221.95	<0.0001
$X_1X_2$	2.81	1	2.81	0.22	0.6428
$X_1X_3$	52.20	1	52.20	4.17	0.0592
$X_1X_4$	118.27	1	118.27	9.44	0.0077
$X_2X_3$	148.23	1	148.23	11.83	0.0036
$X_2X_4$	27.83	1	27.83	2.22	0.1568
$X_3X_4$	2.48	1	2.48	0.20	0.6627
$X_1^2$	606.70	1	606.70	48.44	<0.0001
$X_2^2$	1,128.97	1	1,128.97	90.13	<0.0001
$X_3^2$	421.88	1	421.88	33.68	<0.0001
$X_4^2$	515.30	1	515.30	41.14	<0.0001
Residual	187.88	15	12.53		
Lack of fit	187.33	10	18.77	632.81	<0.0001
Pure error	0.15	5	0.030		
Cor total	17,123.12	29			

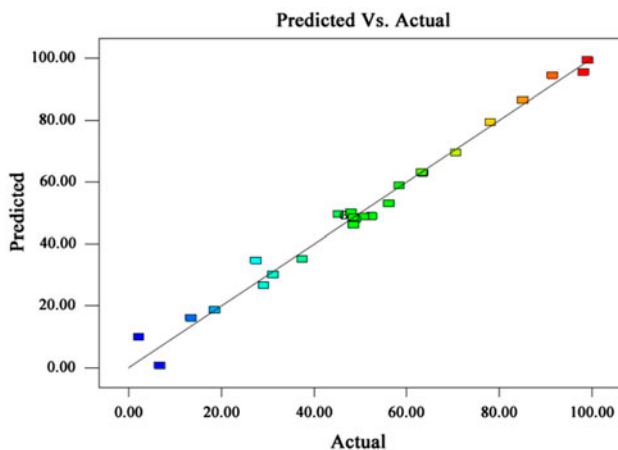


Fig. 5. Correlation of actual and predicted removal efficiency for Ni(II).

Thus, the low Ni(II) removal efficiency under initial strong acidic condition may be attributed to the competition between  $H^+$  and  $Ni^{2+}$  for active adsorption sites. Besides, the  $pH_{pzc}$  of  $NH_2$ -MCM-41 was about 9.72 (Fig. 8(b)), then  $NH_2$ -MCM-41 would be protonated and positively charged under pH 9.72, so the repulsive force between the positively charged  $NH_2$ -MCM-41 and  $Ni^{2+}$  may also inhibit the adsorption of Ni(II). However, when pH increased, some of the adsorption sites would be released and the adsorbent surface could also be deprotonated to some

extent, promoting the adsorption of Ni(II) and increasing the removal efficiency.

In addition, one can see from Fig. 6(a)–(c) that Ni(II) removal efficiency was more than 20% even at very low pH under any fixed metal concentration, temperature, and adsorbent dosage. As to this phenomenon, it can be speculated that cation exchange process between  $Ni^{2+}$  and the  $Al^{3+}$  on the adsorbent surface under acidic condition may also played a role in the removal of Ni(II) [26]. Moreover, at a higher pH, outer-sphere surface complexation maybe significant in the adsorption process [27]. Because a number of  $-NH_2$  existed on the surface of  $NH_2$ -MCM-41, then Ni(II) would complex with  $-NH_2$  on the adsorbent surface, which enhanced the removal of Ni(II). Sun et al. [23] reported that a lone pair of electrons in the nitrogen atom was donated to the shared bond between N and Ni(II) in the X-ray photoelectron spectroscopy analysis on the adsorption of Ni(II) by chitosan.

#### 3.4.2. Effect of temperature

Figs. 6(b) and 7(a) and (c) illustrates the interaction effects of temperature with pH, metal concentration, and adsorbent dosage. It was obvious that Ni(II) removal efficiency increased gradually with increase in temperature, which indicated that high temperature was advantageous for Ni(II) removal. Besides, according to the linear coefficient (+8.50) of  $X_3$  in Eq. (5), a

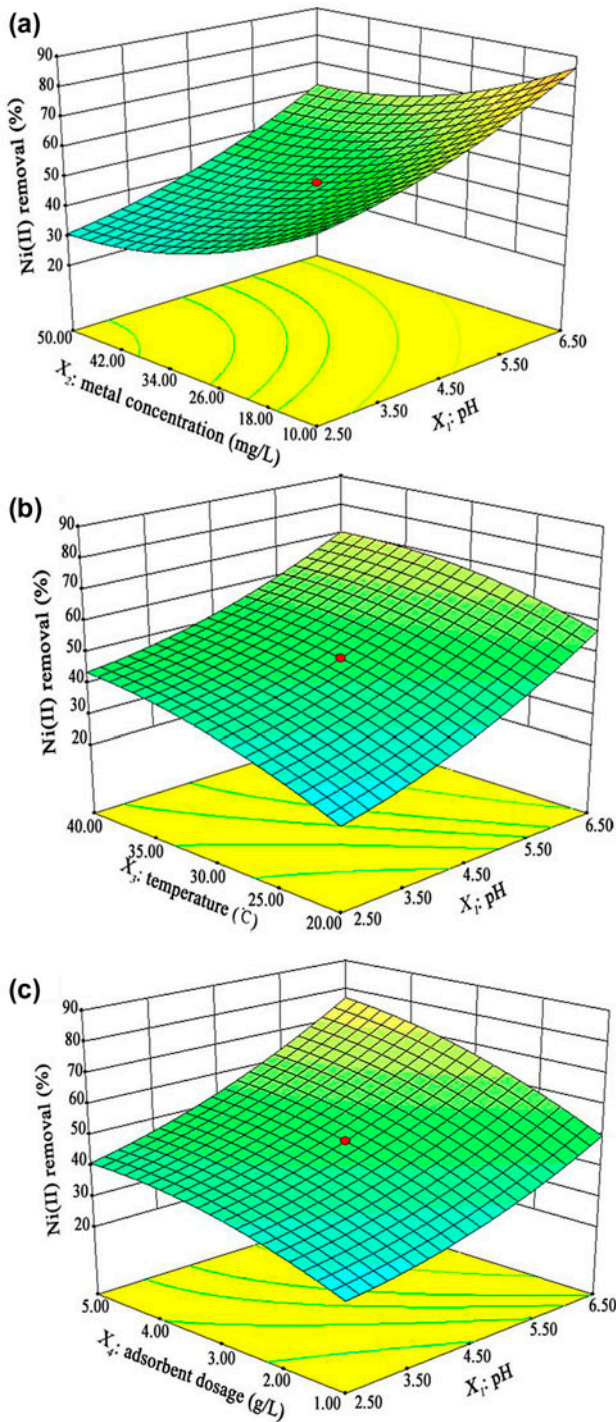


Fig. 6. Response surface plots for the combined effect of initial pH and metal concentration (a), initial pH and temperature (b), initial pH and adsorbent dosage (c) on the removal efficiency of Ni(II).

positive correlation between temperature and the removal efficiency of Ni(II) can be detected. On one

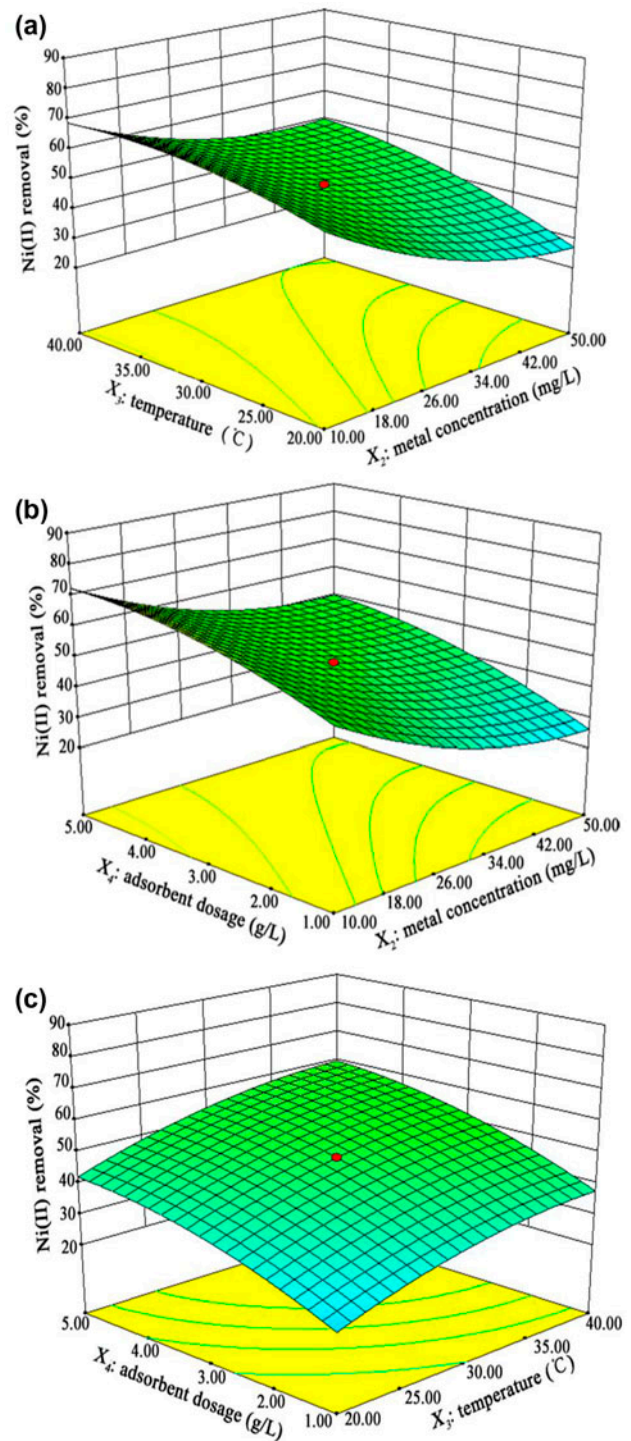


Fig. 7. Response surface plots for the combined effect of metal concentration and temperature (a), metal concentration and adsorbent dosage (b), temperature and adsorbent dosage (c) on the removal efficiency of Ni(II).

hand, higher diffusion rate of Ni(II) across the external layer and into the adsorbent pores due to higher



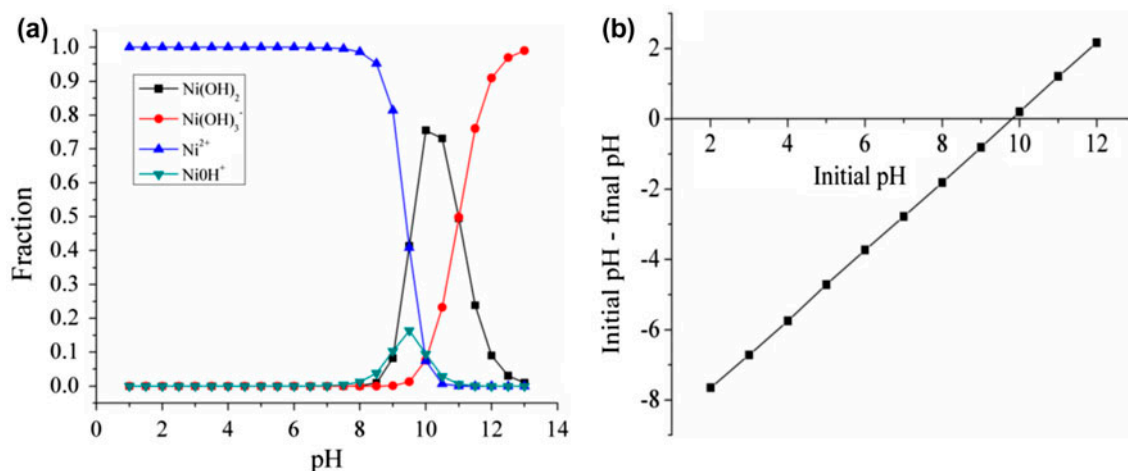


Fig. 8. (a) Diagram for Ni(II) chemical species in aqueous solution and (b) Point of zero charge.

temperature may account for the phenomenon [28]. On the other hand, because of the break of some bonds on adsorbent surface at higher temperature, more available active sites were released, thus enhanced the adsorption of Ni(II).

This situation can be interpreted through the thermodynamic parameters, for example, free energy ( $\Delta G^\circ$ ), enthalpy ( $\Delta H^\circ$ ), and entropy ( $\Delta S^\circ$ ) as well. The  $\Delta G^\circ$ ,  $\Delta H^\circ$ , and  $\Delta S^\circ$  were calculated from the following equations:

$$K_0 = \frac{C_{ad}}{C_e} \quad (6)$$

$$\Delta G = -RT \ln K_0 \quad (7)$$

$$\ln K_0 = \frac{\Delta S^\circ}{R} - \frac{\Delta H^\circ}{RT} \quad (8)$$

where  $K_0$  is the equilibrium constant,  $C_{ad}$  is the amounts of metal ion on adsorbent phase (mg/L),  $R$  is the gas constant (8.314 J/K mol), and  $T$  is the temperature (K).  $\Delta H^\circ$  and  $\Delta S^\circ$  could be obtained from slope and intercept of the van't Hoff plot of  $\ln k_0$  vs.  $1,000/T$ , respectively.

The thermodynamic parameters for adsorption of Ni(II) by NH<sub>2</sub>-MCM-41 are summarized in Table 4. The negative values of  $\Delta G^\circ$  decreased with rise in temperature, implying the adsorption process was spontaneous and higher temperature promoted the adsorption of Ni(II). In addition, the positive value of  $\Delta H^\circ$  meant the adsorption process was endothermic and the positive  $\Delta S^\circ$  indicated affinity of the adsorbent towards Ni(II).

### 3.4.3. Effect of adsorbent dosage

The mutual effects of adsorbent dosage with pH, metal concentration, and temperature are visualized in Figs. 6(c) and 7(b) and (c). The results indicated that the removal percentage increased sharply with rise in adsorbent dosage from 1 to 3.5 g/L. While the increase of adsorbent dosage can hardly improve Ni(II) removal efficiency when it exceeded 3.5 g/L. With a fixed number of Ni(II) in the solution, the more the adsorbent dosage, the more the available adsorption sites were provided. However, when the adsorption process reached equilibrium, the residual Ni(II) in solution was little, and the driving force supplied by concentration gradient could not overcome the transfer resistance [29]. Moreover, there would be more chance of the adsorbent particles to collide with each other, which reduced the available adsorption sites in a certain degree.

### 3.4.4. Effect of metal concentration

As shown in Figs. 6(a) and 7(a) and (b), it can be ascertained that Ni(II) removal efficiency decreased with increasing metal concentration from 10 to 50 mg/L. When metal concentration was low, the adsorbent owned enough adsorption sites, so the removal efficiency was high. Whereas, the adsorption sites would become saturated at a high metal concentration, then the removal efficiency was low.

### 3.5. Confirmation experiments

To support suitability of the model for predicting the optimal condition: pH 6.50, metal concentration

Table 4  
Thermodynamic parameters for the adsorption of Ni(II) by NH<sub>2</sub>-MCM-41

Ion	Temperature(°C)	$\Delta G^\circ$ (kJ/mol)	$\Delta H^\circ$ (kJ/mol)	$\Delta S^\circ$ (J/mol·K)
Ni(II)	25	-1.82	61.62	200.67
	30	-1.92		
	40	-2.04		

10.00 mg/L, temperature 35°C, and adsorbent dosage 5.00 g/L. Confirmation experiment was conducted under the optimal condition and the removal efficiency of Ni(II) reached 93.20%, which was in good agreement with the predicted 95.36% by RSM.

### 3.6. Adsorption isotherms

The study of adsorption isotherms is favorable to understand the relationship between adsorbent and adsorbate as well as provide more information about adsorption capacity of adsorbent. In the present work, the Langmuir, Freundlich, and Dubinin–Radushkevich (D–R) isotherm models were used to analyze the experiment data. The Langmuir model assumes a monolayer adsorption, insists the adsorption sites on adsorbent surface are identical, and there exists no interaction between the adsorbed molecules [30]:

$$q_e = \frac{q_m K_L C_e}{1 + K_L C_e} \quad (9)$$

where  $q_m$  (mg/g) is maximum adsorption capacity of the adsorbent,  $K_L$  (L/mg) presents the Langmuir adsorption constant. The Freundlich isotherm is usually used for assuming an uneven distribution of adsorption heat over the surface, and nonideal multi-layer adsorption [31]:

$$q_e = K_F C_e^{1/n} \quad (10)$$

where  $K_F$  (mg/g) is a constant related to the relative sorption capacity of sorbent,  $n$  is a constant related to the intensity of sorption. The D–R model is mainly used to evaluate adsorption energy [32] and describe the sorption on both homogeneous and heterogeneous surfaces [33]:

$$q_e = q_m \exp(-K_{DR} \varepsilon^2) \quad (11)$$

$$\varepsilon = RT \ln \left( 1 + \frac{1}{C_e} \right) \quad (12)$$

$$E = \frac{1}{\sqrt{2K_{DR}}} \quad (13)$$

where  $K_{DR}$  (mol<sup>2</sup>/kJ<sup>2</sup>) is the constant related to adsorption energy,  $\varepsilon$  is the polanyi potential, and  $E$  (kJ/mol) is the mean free energy of sorption. The adsorption is dominated by chemical ion exchange if  $E$  lies between 8 and 16 kJ/mol, whereas if  $E$  lower than 8 kJ/mol, the adsorption process is of a physical nature [34,35].

Fitted curves of the isotherm models and the corresponding parameters are shown in Fig. 9 and Table 5, respectively. Table 5 gave out the idea that Langmuir was better fitted to the experiment data for the higher  $R^2$  values. Therefore, it can be concluded that the adsorption of Ni(II) may mainly happen on the surface of NH<sub>2</sub>-MCM-41. Moreover, the maximum adsorption capacity was 14.34 mg/g. In comparison with the other adsorbent [1,36–41] as presented in Table 6, NH<sub>2</sub>-MCM-41 had a good adsorption capacity and the potential to be employed in the removal of Ni(II) from solution. The  $E$  values obtained (10.976, 11.890, and 12.909 kJ/mol) were all in the range of 8–16 kJ/mol, indicating the adsorption of Ni(II) was chemical adsorption.

### 3.7. Kinetic study

For purpose of exploring the adsorption mechanism and having a deep insight into the adsorption process, both the pseudo-first-order [42] and pseudo-second-order [43] kinetic models have been used for fitting the experiment data. The linear form of pseudo-first-order (Eq. (14)) and pseudo-second-order (Eq. (15)) model are expressed as follows:

$$\ln(q_e - q_t) = \ln q_e - k_1 t / 2.303 \quad (14)$$

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad (15)$$

where  $q_t$  (mg/g) is the amount of metal ions adsorbed at time  $t$ ,  $k_1$  is the pseudo-first-order adsorption rate

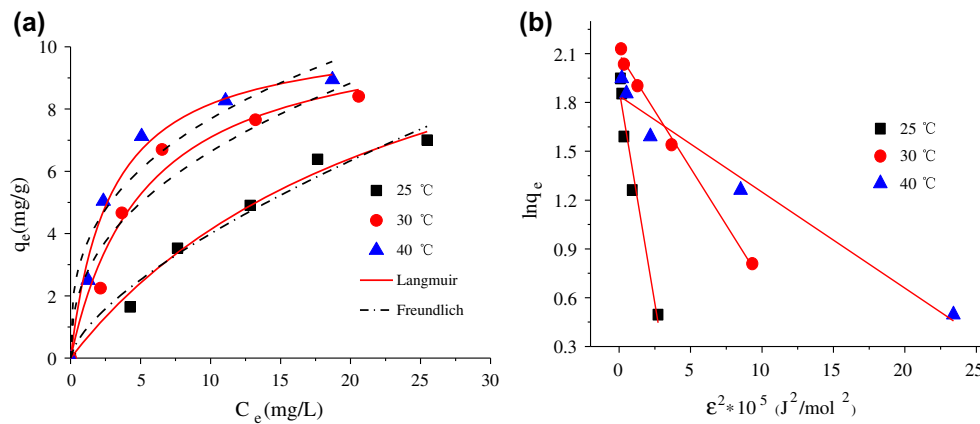


Fig. 9. The fitted curve of isotherm models at different temperature (a) Langmuir and Freundlich and (b) D–R.

Table 5  
Isotherm parameters for the adsorption of Ni(II) by NH<sub>2</sub>-MCM-41

Ion	Temperature (°C)	Langmuir			Freundlich			D–R			
		$Q_0$ (mg/g)	$K_L$	$R^2$	$K_f$	$n$	$R^2$	$Q_m$ (mmol/g)	$K$ (mol <sup>2</sup> /kJ <sup>2</sup> )	$R^2$	$E$ (kJ/mol)
Ni(II)	25	14.34	0.040	0.984	0.862	1.501	0.968	6.546	0.525	0.952	10.98
	30	10.85	0.188	0.968	2.566	2.424	0.924	8.141	0.140	0.964	11.89
	40	10.51	0.347	0.984	3.489	2.915	0.934	6.301	0.059	0.964	12.91

Table 6  
A comparison of adsorption of Ni(II) by different adsorbents

Adsorbent	Adsorption capacity (mg/g)	pH	Concentration (mg/L)	References
Lignocellulosic	2.76	5.8	150	[36]
Rice husk	11.50	6.5	200	[37]
Mixture grafted poly fiber	43.48	5.0	250	[38]
Leonardite	15.26	5.3	230.70	[39]
Brewery's yeast	5.34	6.0	100	[40]
Organic-inorganic silica composites	182	7.0	1,000	[1]
MCM-41	10.25	5.5	40	[41]
NH <sub>2</sub> -MCM-41	14.34	6.5	50	This work

constant (per minute), and  $k_2$  (g/(mg min)) is the pseudo-second-order adsorption rate constant.

The plots of  $\log(q_e - q_t)$  vs.  $t$  (Fig. 10 (a)) and  $t/q_t$  against  $t$  (Fig. 10 (b)) show the suitability of pseudo-first-order and pseudo-second-order kinetic models, respectively. And the related kinetic parameters are listed in Table 7. Comparing with pseudo-first-order kinetic model, pseudo-second-order described the experiment data better for a higher  $R^2$  value. It meant that the rate-limiting step involved chemisorption [44].

Although the above two kinetic model revealed some information about the adsorption process, it could not provide more specific explanation. Therefore, the Spahn and Schlunder model and the intraparticle diffusion model were also employed in the present work. The Spahn and Schlunder model is usually used to describe the external diffusion process, in which the adsorbent across the film to the surface of adsorbent [45]. It can be expressed by the following equation:

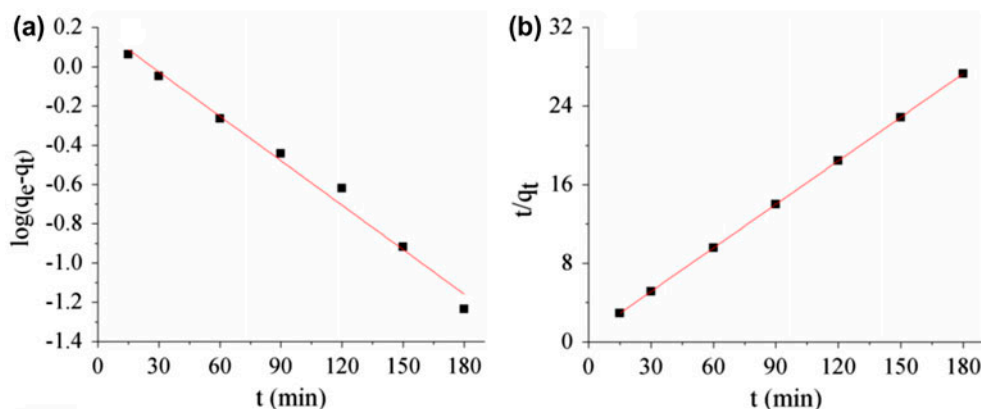


Fig. 10. Pseudo-first-order (a) and pseudo-second-order (b) for the adsorption of Ni(II) by NH<sub>2</sub>-MCM-41.

Table 7  
Kinetic parameters for the adsorption of Ni(II) by NH<sub>2</sub>-MCM-41

Ion Ni(II)	Pseudo-first-order kinetic			Pseudo-second-order kinetic			Intraparticle diffusion model	
	$k_1$ (min <sup>-1</sup> )	$q_e$ (mg/g)	$R^2$	$k_2$ (g/(mg min))	$q_e$ (mg/g)	$R^2$	$k_{2d}$ (mg/(g min <sup>1/2</sup> ))	$k_{3d}$ (mg/(g min <sup>1/2</sup> ))
	0.0167	1.4802	0.9837	0.0306	6.7714	0.9995	0.1779	0.0464

$$\ln C_t = \ln C_0 - k_{\text{ext}}t \quad (16)$$

where  $C_t$  is the metal concentration at time  $t$  in mg/L,  $k_{\text{ext}}$  (1/min) is the external diffusion constant. If external diffusion rate is dominant in the whole adsorption process,  $\ln C_t$  would exhibit a good linear relationship with  $t$ .

Fig. 11(a) shows the relationship of  $\ln C_t$  with  $t$ . In Fig. 11(a), the  $\ln C_t$  had a good linear shape in the initial 60 min, indicating external diffusion was primary in that period.

The intraparticle diffusion model is utilized to represent ion diffusion in the adsorbent micropore [46]:

$$q_t = k_{p,i}t^{0.5} \quad (17)$$

where  $k_{p,i}$  is the intraparticle diffusion rate constant of different stages. In terms of this model, if the paragraph is consist of multilinear, then two or more steps are included in the adsorption process [47].

The paragraph of  $q_t$  vs.  $t^{0.5}$  is presented in Fig. 11(b). As can be seen from Fig. 11(b), the paragraph emerged as three linear parts. The first part represented a extremely fast uptake, which was not shown in the figure. In this part, Ni(II) complexed

with the active sites on adsorbent surface. The second part was by intraparticle diffusion, when the active adsorption sites on adsorbent surface were saturated, then Ni(II) diffused from surface into the micropore. During this period, the mass transfer resistance increased and the adsorption rate was slowed. The third part was the equilibrium stage because of the external or internal adsorption sites were all saturated, thereafter the adsorption process reached equilibrium.

### 3.8. XRF analysis

The chemical composition of NH<sub>2</sub>-MCM-41 is analyzed by XRF and the data are shown in Table 8. The existence of nickel after adsorption was attributed to the complexation of nickel on the adsorbent surface.

### 3.9. Desorption and regeneration studies

In order to make NH<sub>2</sub>-MCM-41 feasible and economical, adsorption–desorption studies were carried out. The result revealed that removal efficiency of Ni (II) decreased slightly along with the times used, and it can still be reached 84% after six times of adsorption–desorption experiments.

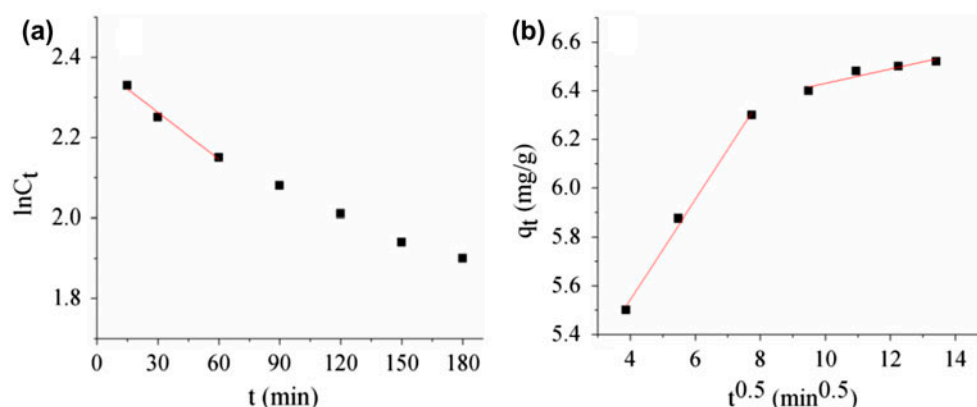


Fig. 11. Spahn and Schlunder model (a) and Intraparticle diffusion model (b) for the adsorption of Ni(II) by NH<sub>2</sub>-MCM-41.

Table 8  
The XRF data of NH<sub>2</sub>-MCM-41 before and after adsorption

	NH <sub>2</sub> -MCM-41	Ni(II)-NH <sub>2</sub> -MCM-41
SiO <sub>2</sub> (m/m%)	93.03	93.25
Al <sub>2</sub> O <sub>3</sub> (m/m%)	5.56	4.70
NiO (m/m%)	0	0.95

#### 4. Conclusions

RSM was used to optimize the adsorption of Ni(II) using NH<sub>2</sub>-MCM-41. The solution pH, metal concentration, temperature, and adsorbent dosage significantly influence Ni(II) removal efficiency, while the maximum value (93.20%) was achieved at 6.50, 10.00 mg/L, 35 °C, and 5.00 g/L, respectively. Langmuir model depicted the experiment data better and the maximum adsorption capacity was 14.34 mg/g. The kinetic data showed the adsorption of Ni(II) fitted well with pseudo-second-order model. Moreover, the intraparticle diffusion model indicated three stages of the adsorption process: fast uptake, intraparticle diffusion, and equilibrium stage. The calculated thermodynamic parameters hinted the adsorption of Ni(II) by NH<sub>2</sub>-MCM-41 was feasible, endothermic, and spontaneous. Besides, NH<sub>2</sub>-MCM-41 can be a potential adsorbent for Ni(II).

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