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Removal of potassium permanganate from water by modified carbonaceous materials

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ABSTRACT

Potassium permanganate is commonly used in multidiscipline processes as a strong oxidizing agent for oxidative treatment of a great number of organic and inorganic compounds. In this work, a method is proposed for removal of KMnO₄ from aqueous solutions and real water samples using treated and activated carbon (AC) sorbents with sulfuric acid. The potential applications of five modified AC sorbents for removal of KMnO₄ were explored under different experimental controlling factors including pH, contact time, initial concentration of KMnO₄, sorbent dosage, and competing ions by the batch equilibrium technique. The removal values of KMnO₄ removal from aqueous solutions was found to proceed by an anion exchange and ion pair interaction mechanisms, while in pH \geq 3.0–7.0, the uptake of KMnO₄ was identified to take place by an initial surface reduction step for the formation of Mn(II) ion and followed by adsorption via a direct complex formation with the AC surface functional groups. The proposed method confirmed an efficient removal of \geq 99% of residual KMnO₄ from industrial wastewater, seawater, and drinking water in laboratory trials.

Keywords: Potassium permanganate; Carbonaceous materials; Removal

1. Introduction

Potassium permanganate (KMnO₄) is well known as a strong oxidizing agent and has been characterized for its efficient reaction with electron-rich organic and inorganic compounds. The redox reaction involving KMnO₄ may proceed via several mechanisms and pathways, including direct oxygen transfer, electron exchange, and hydrogen abstraction [1]. Oxidation reactions involving KMnO₄ are also dependent on the pH value of contact solution. In strong acidic medium, KMnO₄ exhibits high oxidative reactivity with oxidation potential ($E^{\circ} = +1.51$ V) and its reductive product is the Mn²⁺ according to equation Eq. (1). On the other hand, KMnO₄ undergoes in acidic–neutral and alkaline pH conditions to produce manganese dioxide with $E^{\circ} = +0.59$ and +1.70 V, respectively, as illustrated by Eqs. (2) and (3) [2].

In strong acidic condition:

 $MnO_4^- + 8H^+ + 5e^- \rightarrow Mn^{2+} + 4H_2O$ (1)

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In acidic-neutral condition:

 $MnO_4^- + 4H^+ + 3e^- \rightarrow MnO_2(s) + 2H_2O$ (2)

In alkaline condition:

$$MnO_{4}^{-} + 2H_{2}O + 3e^{-} \rightarrow MnO_{2}(s) + 4OH^{-}$$
 (3)

Due to the strong oxidizing power of permanganate in various solutions, $KMnO_4$ was widely used in chemical oxidation treatment processes of water and soil to remediate organic and inorganic pollutants [3]. In addition, water treatment using $KMnO_4$ was established to replace chlorine treatment in which $KMnO_4$ was used as a pre-oxidation step to react with dissolved organic matters due to its potential capability for elimination of the chlorinated byproducts. Moreover, $KMnO_4$ was also used in drinking water treatment to improve the removal efficiency of contaminants [4].

A number of research papers have been recently reported on the application of KMnO₄ as a strong, efficient, and relatively low-cost oxidizing reagent for removal of organic pollutants from aqueous solutions and water samples [1,5-8]. A study was aimed and reported to develop hypersaline MnO₄⁻ solution (MnO₄⁻ gel; PG) that was injected into aquifers via wells and found to release MnO_4^- to the flowing water [9]. Batch experiments were carried out to investigate the decomposition of bisphenol A (BPA) by permanganate and the proposed method was found very effective for BPA degradation by producing over 99% remediation of BPA after 15 min at pH 7.0 [10]. Benchscale experiments were investigated to monitor the potassium permanganate demand and its variation with depth in PAHs contaminated site of a coking plant [11]. The effect of permanganate pre-oxidation on organic matter removal during the coagulation with aluminum chloride using tannic acid as a model compound was investigated and reported [12]. Activated carbon (AC) adsorbent was prepared and treated with KMnO4 for removal of Basic Violet 14 from aqueous solutions [13]. A method was presented to find out the effects of KMnO₄ on powdered AC in the treatment and removal of natural organic matter [14].

Oxidative removal of various inorganic species was also reported by a number of research papers. A method was described for oxidation of As(III) by means of four conventional oxidants (chlorine dioxide, sodium hypochlorite, potassium permanganate, and monochloramine) under different test conditions [15]. A three-step method was reported as a treatment process for simultaneous removal of arsenic and iron ions from water involving (i) mild alkaline pH-conditioning by NaHCO₃, (ii) oxidation of arsenite and ferrous ions by KMnO₄, and (iii) coagulation by FeCl₃ [16]. A method was also reported for simultaneous removal of SO₂, NO and Hg^o from flue gas using a complex absorbent containing KMnO₄ and under the influence of different types of oxidants, urea concentration, KMnO₄ concentration, Hg^o inlet concentration, initial pH, reaction temperature as well as SO₂ and NO concentrations [17].

AC adsorbents have been widely used in combination with KMnO₄ in water treatment processes [13,14]. However, in such combined treatment methodology, a direct contact reaction is favored between KMnO₄ and AC as well as the removed organic or inorganic adsorbate. If potassium permanganate is present in excess, the surface functional groups will change due to possible redox reaction for the formation of some other surface functional groups such as carboxyl, hydroxyl, ketonic, and ether as previously reported [18–20]. The physical and chemical characteristics of AC adsorbent oxidized by KMnO₄ were also studied to evaluate the relationship between oxidant and adsorption process in drinking water treatment as reported in several research papers [13,14,21].

Removal of manganese species from water is mainly focused on only manganese (II) ion [22-33]. However, limited data are available concerning KMnO₄ toxicity to untargeted species in water systems. In addition, no standard pattern for applications of KMnO₄, and therefore it can be used without restriction. Therefore, implementation of KMnO₄ as a strong oxidizing agent in water treatment plants will require additional studies [34]. To the best of our knowledge, the potential application of AC for removal of trace amounts of KMnO4 from water and aqueous solutions was not previously reported. Therefore, the aim of this study is mainly focused on the removal processes of KMnO₄ from aqueous solutions and real water samples using chemically treated AC adsorbents with $0.1-1.0 \text{ mol } \text{L}^{-1}$ sulfuric acid. The influence of different experimental controlling factors was also studied, optimized, and evaluated in this study.

2. Experimental

2.1. Materials and methods

All chemicals were of analytical or laboratory grade reagents. Potassium permanganate (KMnO₄, 99% purity) was purchased from Biochem for laboratory chemicals and used to freshly prepare a 1,000 mg L^{-1} stock solution. Sulfuric acid (97%) and

other metal salts were purchased from Sigma-Aldrich, Germany. Powdered commercial AC was purchased from Adwic Chemicals, Egypt, and used as received.

2.2. Preparation of modified AC sorbents

Powdered AC was treated with distilled water by heating and stirring at 110°C for 1 h in order to remove surface-adsorbed contaminants. The washed AC sorbent was filtered and left to dry in an oven at 60–70°C for complete dryness. A sample of 10.0 g of dry AC was weighed and transferred to a 250.0 mL beaker containing 100.0 mL of $0.1 \text{ M-H}_2\text{SO}_4$ and the reaction mixture was slowly stirred for 3 h, then filtered, washed with distilled water, and dried at 70°C to produce the AC-1.0 M sorbent. The same procedure was also repeated using different molar concentrations of sulfuric acid such as 0.3, 0.5, 0.7, and 1.0 M to produce AC-0.3 M, AC-0.5 M, AC-0.7 M, and AC-1.0 M sorbents, respectively.

2.3. Stability of modified AC sorbents

The stability of modified AC sorbents in aqueous solutions was performed according to the following procedure. A 50 ± 1.0 mg sample of AC-0.1 M, AC-0.3 M, AC-0.5 M, AC-0.7 M, or AC-0.1 M sorbent was added to 50.0 mL of distilled water. This mixture was shaken by automatic shaker for 30 min and filtered, and the filtrate was titrated against standard 0.1 M-sodium hydroxide. The percentage value of leached sulfuric acid from each modified sorbent was determined based on triplicate analysis.

2.4. Sorption studies

2.4.1. Reduction of $KMnO_4$ by modified AC sorbents

A $50.0 \pm 1.0 \text{ mg}$ sample of modified AC sorbent was added to a mixture of 10.0 mL of 0.01 M-KMnO_4 solution into a 50.0 -mL measuring flask. This mixture was shaken for 30 min by an automatic shaker (125 rpm). The mixture was filtered and washed with 50.0 mL of distilled water. $100 \pm 1.0 \text{ mg}$ of oxalic acid was added to the filtrate, boiled for few minutes and hydroxylamine HCl was then added. The pH value of this solution was adjusted to pH 10.0 and the unextracted Mn(II) in the filtrate was determined by complexometric titration against 0.01 M-EDTA using Erio-T indicator.

2.4.2. UV-vis spectrophotometric analysis of KMnO₄

According to the operational manual of the UV-vis spectrophotometric determination, adjustments of the

instrument parameters gave optimized conditions for the work done. The absorbance full curve of KMnO₄ was acquired and found to produce three peaks at 480, 525, and 580 nm and the maximum absorbance was identified at $\lambda = 525$ nm [35]. This wavelength was then used to establish the calibration curve as represented in Fig. 1 by fitting the absorbance against concentration at this specified wavelength of maximum absorption. In addition, $\lambda = 525$ nm was also used to determine the concentration of KMnO₄ as described below.

2.4.3. Effect of pH

All batch sorption experiments were carried out at room temperature ($25 \pm 1^{\circ}$ C). Each experiment was performed in a 50 mL volumetric flask by mixing a 10.0 mL of 100.0 mg L⁻¹ freshly prepared KMnO₄ solution with 50.0 ± 1.0 mg of the dry AC sorbent and the pH was adjusted in the range of 1.0–7.0 by the addition of either H₂SO₄ or NaOH. This mixture was shaken by an automatic shaker (125 rpm) for 30.0 min and finally filtered. Residual KMnO₄ in the filtrate was detected using UV–vis spectrophotometric determination at $\lambda = 525$ nm. The percentage removal of KMnO₄ was calculated according to Eq. (4).

Removal efficiency (%) =
$$\frac{C_{\rm o} - C_{\rm e}}{C_{\rm o}} \times 100$$
 (4)

where C_0 and C_e are the initial and final concentrations of KMnO₄ expressed in mg L⁻¹, respectively.





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2.4.4. Effect of contact time

The previously mentioned batch experiment procedure was also carried out at different shaking time values, viz. 1.0, 5.0, 10.0, 15.0, 20.0, 25.0, and 30.0 min and the optimum pH 1.0 and 7.0 were adjusted using H₂SO₄ or NaOH solution. The residual KMnO₄ in the filtrate was detected using UV–vis spectrophotometric determination at $\lambda = 525$ nm and the percentage removal of KMnO₄ at each time value was calculated from Eq. (4).

2.4.5. Effect of sorbent dosage

Similar batch experiments were carried out by mixing a 10.0 mL freshly prepared solution of 100.0 mg L⁻¹ KMnO₄ using different sorbent masses, 2.0, 5.0, 10.0, 20.0, 40.0, 60.0, 80.0, and 100.0 ± 1.0 mg. The optimum pH 1.0 and 7.0 were adjusted by H₂SO₄ or NaOH solution. The mixture, in each case, was shaken for 30.0 min by an automatic shaker (125 rpm) and the residual KMnO₄ in the filtrate was detected using UV–vis spectrophotometric determination at λ = 525 nm and the removal percentage of KMnO₄ was evaluated from Eq. (4).

2.4.6. Effect of initial metal concentration

Freshly prepared solutions (10.0 mL) with 10.0, 20.0, 30.0, 40.0, 50.0, 60.0, 70.0, 80.0, 90.0, and 100.0 mg L⁻¹ KMnO₄ were used to conduct this study. These solutions were mixed with 20.0 ± 1.0 mg of the dry AC sorbent, adjusted to pH 1.0 and 7.0, and shaken for 30 min (125 rpm). The mixture was filtered and the residual KMnO₄ in the filtrate was detected using UV–vis spectrophotometric determination at $\lambda = 525$ nm. The percentage removal of KMnO₄ was determined from Eq. (4).

2.4.7. Effect of interfering ion

Several selected metal salts such as Na₂SO₄, MgSO₄, CaSO₄, ZnSO₄, NiSO₄, and (NH₄)₂SO₄ were used to study the effect of coexisting ions on the percentage removal of KMnO₄ using various modified AC sorbents. The solutions were prepared by mixing 10.0 mL of 100.0 mg L⁻¹ KMnO₄ with 10.0 ± 1.0 mg of the interfering salt and 50 ± 1.0 mg of the dry AC sorbent was then added in a 50 mL volumetric flask. The optimum pH 1.0 was adjusted by adding H₂SO₄ and the sorption mixture was shaken for 30.0 min (125 rpm) and filtered. The residual KMnO₄ in the filtrate was detected using UV–vis spectrophotometric determination at $\lambda = 525$ nm. The percentage removal

of KMnO₄ was evaluated from Eq. (4). For successful comparison, the previous experiment was evaluated in the absence of the interfering ion. The same previous removal procedure was also repeated at pH 7.0.

2.4.8. Application of modified AC sorbents for removal of KMnO₄ from various water samples

500 mL of the tested tap water, sea water, and industrial wastewater samples were spiked with 5.0 mg L⁻¹ KMnO₄ and adjusted to pH 1.0 and 7.0 by the addition of H₂SO₄ or NaOH solution. These were mixed with 100.0 ± 1.0 mg of the dry AC sorbent and shaken for 30 min. The residual KMnO₄ in solution was filtered and detected using UV–vis spectrophotometric determination at λ = 525 nm. The removal value of KMnO₄ was calculated from Eq. (4).

3. Results and discussion

3.1. Surface modification and characterization

In this work, AC was treated with various concentrations of sulfuric acid, viz. 0.1, 0.3, 0.5, 0.7, and $1.0 \text{ mol } L^{-1}$ to produce AC-0.1 M, AC-0.3 M, AC-0.5 M, AC-0.7 M, and AC-1.0 M sorbents, respectively. The stability of loaded sulfuric acid on the surface of AC sorbents in aqueous solution was determined by direct shaking of these sorbents in distilled water. The leached amount of sulfuric acid was then titrated against standard 0.1 M sodium hydroxide. The identified percentage values of leached sulfuric acid from the surface of modified AC sorbents were determined on the basis of triplicate analysis and found in the range of $7.4-12.5 \pm 1.5\%$.

The modified AC sorbents were characterized using various instrumental methods of analysis such as Fourier transform infrared (FT-IR) and scanning electron microscope (SEM) as effective techniques for structural characterization and evaluation of the surface morphology. Fig. 2(a)–(c) shows the FT-IR spectra of free AC, AC-0.1 M, and AC-1.0 M, respectively. The spectra were recorded in the FT-IR range 400-4,000 cm⁻¹. As shown in Fig. 2(a), the spectrum of AC sorbent is referring to the complex nature of this sorbent and is characterized by the presence of a number of peaks. A broad peak at 3,405 cm⁻¹ is mainly related to the O-H stretching bond or adsorbed water molecule as previously reported [36,37]. The observed peak at 2,923 cm⁻¹ could be assigned to the aliphatic CH-stretching frequency. The peak at $1,614 \text{ cm}^{-1}$ is mainly due to the formation of oxygen functional groups based on highly conjugated C=O stretching in carboxylic or carboxylate as well as carbonyl groups



Fig. 2. FT-IR spectrum of various AC sorbents.

[38]. Another peak centered at 1,165 cm⁻¹ is assigned to the frequency of C–O bond in methoxyl group. The assigned peak at 1,460 cm⁻¹ is ascribed to the presence of δ (C–H) from methyl groups [39]. Some other peaks appear in the range of 590–1,052 cm⁻¹ and these could be assigned to the =C–H band similar to alkenes.

The SEM images of free AC, AC-0.1 M, and AC-1.0 M sorbents are represented in Fig. 3(a)–(c), respectively. Fig. 3(a) shows the SEM image of AC sorbent using 2,000 magnification order and the particles are distributed in a homogenous fashion with

different shapes and sizes. On the other hand, Fig. 3(b) and (c) represents the image of treated AC sorbent with 0.1 and 1.0 M sulfuric acid using 5,000 magnification order. Some pores were characterized







Fig. 3. SEM images of various AC sorbents.

especially in Fig. 2(c) which indicate a good possibility for the adsorption and trapping of the interacting adsorbate.

3.2. Uptake of KMnO₄ and adsorptive removal of Mn(II) by various AC sorbents

A study was made to confirm the possible removal of Mn(II) as the reduction product of KMnO₄ from aqueous solutions by various treated AC sorbents. The direct contact of KMnO4 with modified AC sorbent was examined for the formation of Mn(II) as the reduction product of KMnO₄. The produced Mn(II) was evaluated for its adsorptive removal by AC sorbents and the results of this study are compiled in Table 1. It is important to report that the color of solution upon reaction of KMnO4 with modified AC sorbents was turned to colorless and this behavior refers to the complete removal of KMnO₄ via three different mechanisms. The first one is related to an anion exchange mechanism in which a direct adsorptive exchange of MnO_4^- by the loaded SO_4^{2-} on the surface of AC sorbents in the presence of low pH values of contact solution (pH 1.0-2.0) [28]. In addition, the second possible mechanism may be related to the formation of ion pairing between MnO₄⁻ and surface protonated groups. The percentage removal values of KMnO₄ by these two mechanisms are characterized as 36.0, 43.0, 44.6, 46.2, and 50.0% by AC-0.1 M, AC-0.3 M, AC-0.5 M, AC-0.7 M, and AC-1.0 M sorbents, respectively. The third mechanism is mainly due to the reduction reaction of KMnO₄ to produce Mn(II) in solution which is then adsorbed by the surface functional groups of AC sorbents via a complex formation reaction in the contact solutions with $pH \ge 3.0$. Thus, it is evident from the listed data that a reduction process of KMnO₄ was taken place and the modified AC sorbents were found to produce 97.30-100.0% reduction and adsorptive removal of Mn(II) from aqueous solution in pH 7.0. In addition, a gradual increase in the percentage extraction values of Mn(II) by all AC sorbents was also evident by the increase in the pH value of contact solution. This behavior is mainly due to the strong capability of Mn(II) to bind and form complexes with the active surface functional groups such as OH, COOH, and C=O [38].

3.3. Adsorptive removal of $KMnO_4$ -Mn(II) by modified AC sorbents in the presence of various controlling parameters

3.3.1. Effect of pH on the adsorptive removal of KMnO₄-Mn(II)

The effect of pH value of contact solution on the removal process of KMnO4-Mn(II) was studied in various acidic and neutral solutions with (pH 1.0-7.0) and the results of this study are listed in Table 2. The percentage extraction values of KMnO4 were found to be \geq 99.55% in all aqueous solutions by the examined AC sorbents. In pH 1.0 solution, removal of KMnO₄ was found to proceed via anion exchange mechanism by producing percentage extraction values ≥99.66–99.95%. At higher pH value (pH 7.0), the percentage extraction of Mn(II) as the reduction product of KMnO₄ was found in the range of 99.65-99.93% due to the possibility of complex formation as described in Section 3.2. Therefore, the listed data in Table 2 refer to the excellent recovery values of KMnO₄ from aqueous solutions in the pH range 1.0-7.0.

3.3.2. Effect of contact time on the adsorptive removal of KMnO₄–Mn(II)

The effect of contact time on the percentage extraction of $KMnO_4$ -Mn(II) was also studied and evaluated in this section in order to find out the

рН	% Removal of KMnO ₄ -Mn(II) by modified AC-H ₂ SO ₄ sorbents ^a						
	AC-0.1 M	AC-0.3 M	AC-0.5 M	AC-0.7 M	AC-1.0 M		
1	12.90	34.40	36.60	38.70	43.00		
2	36.00	43.00	44.60	46.20	50.50		
3	80.10	80.60	81.20	84.40	84.90		
4	82.30	83.90	90.90	92.50	95.20		
5	94.60	95.20	96.20	97.30	97.30		
6	96.20	97.30	97.30	98.40	99.50		
7	97.30	97.80	98.40	98.90	100.0		

Table 1 Percentage extraction values of KMnO₄–Mn(II) by modified AC sorbents

^aValues are based on triplicate analysis with ±1.0%.

∂								
рН	% Extraction of KMnO ₄ –Mn(II) in different pH values ^a							
	AC-0.1 M	AC-0.3 M	AC-0.5 M	AC-0.7 M	AC-1.0 M			
1	99.66	99.76	99.87	99.93	99.95			
2	99.55	99.66	99.75	99.82	99.89			
3	99.56	99.61	99.74	99.81	99.89			
4	99.56	99.61	99.74	99.81	99.90			
5	99.56	99.61	99.74	99.81	99.90			
6	99.61	99.65	99.76	99.85	99.90			
7	99.65	99.73	99.85	99.88	99.93			

Table 2 Percentage extraction values of KMnO₄-Mn(II) in different pH solutions

^aValues are based on triplicate analysis with ±1.0%.

removal rapidness of both species, KMnO₄ and Mn (II). This factor was accomplished using two different pH values, 1.0 and 7.0, to monitor the adsorption progress of KMnO₄ and Mn(II), respectively. The time interval values were selected as 1.0, 5.0, 10.0, 15.0, 20.0, 25.0, and 30.0 min for both cases. The results of this study are represented in Fig. 4(a) and (b) at pH 7.0 and 1.0, respectively. The uptake process of KMnO₄ in pH 1.0 was found very fast due to almost complete removal after only one minute of contact time. The identified percentage values of KMnO₄ by all modified AC sorbents were found to be ≥99.45% and this confirms the efficient application of modified AC sorbents for removal of KMnO4 from aqueous solutions. In pH 7.0, the AC sorbents were also found to exhibit excellent recovery values of Mn(II) as the reduced ion of KMnO₄. After one min of contact time, the identified values for removal of Mn(II) from aqueous solution by AC-0.1 M, AC-0.3 M, AC-0.5 M, AC-0.7 M, and AC-1.0 M were found as 99.32, 99.45, 99.50, 88.58, and 99.67%, respectively.

The results of this study confirm that the evaluated AC sorbents are highly efficient in removal of $KMnO_4$ and Mn(II) from adjusted aqueous solutions at pH 1.0 and 7.0, respectively.

3.3.3. Effect of sorbent dose on the adsorptive removal of $KMnO_4$ -Mn(II)

The effect of sorbent dosage on the removal of KMnO₄ and Mn(II) by modified AC in the range of 2.0–100.0 mg and using 100 mg L⁻¹ as the initial concentration sorbents was also studied as an important factor by varying the selected sorbent dosages of KMnO₄. The selected contact time was adjusted to 30.0 min and the results of sorbent dosage on the removal efficiency of modified AC sorbent for Mn(II) in pH 7.0 and KMnO₄ in pH 1.0 are graphed in



Fig. 4. Effect of contact time on the removal process of Mn (II) from different pH values. (a) Effect of contact time (pH 7.0), and (b) effect of contact time (pH 1.0).

Fig. 5(a) and (b), respectively. The AC sorbent dosage was found to exhibit a slight increase in the percentage extraction values of $KMnO_4$ from pH 1.0 and Mn (II) from pH 7.0 solution upon increasing the sorbent

dosage. A 2.0 mg of sorbent dosage was found to produce 97.20–97.85% for $KMnO_4$ removal from pH 1.0. Moreover, the percentage recovery of Mn(II) from pH 7.0 solution using a 2.0-mg dosage of all evaluated AC sorbents was characterized in the range of 97.18–97.85%. The collected data refer to the high efficiency of modified AC sorbents to afford complete uptake (99.32–99.88%) and (99.25–99.75%) of KMnO₄ and Mn(II), respectively, using only 10.0 mg of the examined AC sorbents.

3.3.4. Effect of initial concentration of $KMnO_4$ on the adsorptive removal of $KMnO_4$ –Mn(II)

The effect of different initial concentrations of $KMnO_4$ on the removal efficiency of $KMnO_4$ and Mn (II) using modified AC sorbents was evaluated by varying the concentration of $KMnO_4$ in the range of 10.0–100.0 mg L⁻¹. The sorbent dosage was selected as 2.0 mg and shaking time was adjusted to 30 min. The results of this study are represented in Fig. 6 and

clearly show excellent and complete percentage extraction and uptake values of KMnO₄ from pH 1.0 by all studied and evaluated AC sorbents. The same behavior was also characterized for removal of Mn(II) from pH 7.0 as the reducing product by all AC sorbents. A slight decrease in the extraction values was evident upon increasing the concentration of KMnO₄ from 10.0 to 100.0 mg L⁻¹ and the minimum identified percentage range of KMnO₄ was 97.18–97.89% (pH 1.0) and that of Mn(II) was 97.10–97.81% (pH 7.0).

3.3.5. Effect of interfering ions on the adsorptive removal of KMnO₄–Mn(II)

The effect of interfering cations such as Na(I), Mg (II), Ca(II), Ni(II), Zn(II), and NH_4^+ as well as anion such as SO_4^{2-} in the form of Na₂SO₄, MgSO₄, CaSO₄, ZnSO₄, NiSO₄, and (NH₄)₂SO₄ were used to evaluate the removal processes of KMnO₄ from pH 1.0 and Mn (II) from pH 7.0 by all modified AC sorbents. In this study, a 10.0 mg sample of the interfering salt was





Fig. 5. Effect of AC sorbent dosage on the removal process of Mn(II) from different pH values. (a) Effect of AC sorbent dosage (pH 7.0) and (b) effect of AC sorbent dosage (pH 1.0).

Fig. 6. Effect of initial concentration of $KMnO_4$ on the percentage extraction values of Mn(II) in different pH values. (a) Effect of initial concentration of $KMnO_4$ (pH 7.0) and (b) effect of initial concentration of $KMnO_4$ (pH 1.0).

	% Extraction of KMnO ₄ in the presence of interfering compound ^a					
Interfering species	AC-0.1 M	AC-0.3 M	AC-0.5 M	AC-0.7 M	AC-1.0 M	
Na ₂ SO ₄	99.65	99.63	99.81	99.84	99.73	
MgSO ₄	99.65	99.63	99.74	99.84	99.20	
CaSO ₄	99.60	99.63	99.87	99.93	99.80	
ZnSO ₄	99.65	99.56	99.74	99.93	99.73	
NiSO ₄	99.60	99.47	99.87	99.84	99.80	
$(NH_4)_2SO_4$	99.60	99.56	99.81	99.64	99.53	
Absence of interference	99.65	99.76	99.87	99.93	99.94	

Table 3 Effect of interfering species on the percentage extraction values of KMnO₄ at pH 1.0

^aValues are based on triplicate analysis with ±1.0%.

Table 4 Effect of interfering species on the percentage extraction values of Mn(II) at pH 7.0

	% Extraction of Mn(II) in the presence of interfering species ^a					
Interfering species	AC-0.1 M	AC-0.3 M	AC-0.5 M	AC-0.7 M	AC-1.0 M	
Na ₂ SO ₄	99.65	99.73	99.85	99.88	99.84	
MgSO ₄	99.65	99.67	99.64	99.81	99.92	
CaSO ₄	99.57	99.73	99.75	99.81	99.92	
ZnSO ₄	99.65	99.57	99.85	99.88	99.92	
NiSO ₄	99.57	99.67	99.75	99.81	99.84	
$(NH_4)_2SO_4$	99.62	99.73	99.64	99.88	99.84	
Absence of interference	99.65	99.73	99.85	99.90	99.93	

^aValues are based on triplicate analysis with ±1.0%.

added to KMnO₄ solution and the experimental procedure was completed under the optimum conditions of contact time and sorbent dosage. The presence of interfering ions in aqueous solutions with pH 1.0 and 7.0 was found to maintain the effectiveness of all AC sorbents to react and bind with KMnO₄ and Mn(II), respectively. It is also evident that no direct interaction or contribution of the interfering ions in the adsorption process as listed in Tables 3 and 4.

3.4. Applications of modified AC sorbents for removal of KMnO₄ from real water samples

The capability and efficiency of modified AC sorbents to remove KMnO₄ from real water samples such as industrial wastewater, sea water, and drinking tap water were further studied and evaluated by the batch equilibrium technique as the final and most important step to examine their potential applications in water treatment. In this study, a 100.0 ± 1.0 mg sample of AC sorbent was added to the selected water sample and spiked with trace concentration of 5.0 mg L⁻¹ of KMnO₄. The pH value of these water samples was

adjusted to pH 1.0 and 7.0. The selected contact time was 30.0 min. The percentage extraction values of the spiked 5.0 mg L⁻¹ of KMnO₄ in the examined industrial wastewater, sea water, and drinking tap water samples by all modified AC sorbents were found to correspond to 99.4–100.0 \pm 1.0% and these results give additional evidences for the suitable implementation of modified AC sorbents for removal of existing KMnO₄ from any water sample or matrix.

4. Conclusion

The modified AC sorbents were found to be highly efficient for removal of KMnO4 from aqueous solutions and real water samples in the presence of pH 1.0-7.0. Adsorptive removal of KMnO₄ from pН 1.0-2.0 was suggested to take place by ion pair interaction and anion exchange mechanisms. Removal of KMnO₄ in the presence of pH 3.0-7.0 was found to proceed via reduction of Mn(II) and complex formation of this ion with the surface functional groups. Adsorptive removal of KMnO₄ was found very fast and nearly complete after one minute of contact time in both pH 1.0 and 7.0. The percentage extraction values for removal of KMnO₄ from industrial wastewater, sea water, and drinking tap water were found to be 100.0 $\pm 0.5\%$.

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