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# Modeling of adsorption isotherms of (5,5'-disodium indigo sulfonate) from aqueous solution onto activated carbon: equilibrium, thermodynamic studies, and error analysis

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es (5,5'-disodium indigo sulfonate, The activated carbon (AC) and its ab y to C) use to re Indigotine I, blue CI n°1, Indigo carmine l tex and biology from aqueous solution eters of are investigated. The kinetic and eq ibri par Atative adsorption for IC removed by AC were studied by UV-visi absorptio pectros y. The present work deals with the adsorption of IC dyes on AC, affecting the adsorption capacity were he effects o ramet determined to find the optima ditions for ng the maximum amount of adsorption. The physicochemi characterized by BET method and point of ha cteri of the AC we zero charge. The adon mecha of IC onto AC was studied; the adsorption kinetics was found to follow a pa netic model. The equilibrium adsorption data for IC on econd-ord nodels. Ti AC were analyzed by sev aller root mean square error values for the Langmuir and Dubinin-Radushkevich els indica. the best fitting; the monolayer adsorption capacity of d 298.34 mg/g at 40°C at pH 2. The adsorption isotherms IC was found 19 mg/g ed to obtain thermodynamic parameters: the free energy at differe mpera have t  $(\Delta G^{\circ} =$ g/mol), enthalpy ( $\Delta H^\circ$  = 28.11 kJ/mol), and entropy ( $\Delta S^\circ$  = 0.093 kJ/mol K) of 1 to -1.0adsorpti ctiva energy  $E_a$  of 51.06 kJ/mol. The negative  $\Delta G^{\circ}$  and positive  $\Delta H^{\circ}$  values with tb erall ac ption is spontaneous and endothermic. This study in tiny batch gave ndicate ing result to en d we wish to achieve the adsorption tests in column mode under the treatment of industrial effluents, and the present investigation showed ditions able to AC is a pe eful adsorbent for the dyes.

unords: Indigotine; Removal; Kinetics; Equilibrium; Thermodynamics; Modeling; Isotherm;

## 1. Intinition

Dyes a commonly used in many industries, like textile, food, pan, plastic, cosmetics, and coloring industries. These industries commonly use synthetic dyes as colorants. Discharge of dyes contained in wastewaters contaminates both the surface water and ground water. However,  $7 \times 10$  t of dye stuff are produced annually. The dyes even at very low concentrations affect the aquatic life and human health by polluting the environment. The toxicity and carcinogenicity have lead to exploration of possible detoxicants. Dyes can cause allergies, dermatitis, skin irritation, cancer, mutation, etc. In general, dyes are poorly biodegradable, and some of them produce aromatic amines which are highly

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carcinogenic. Many investigators have studied the feasibility of inexpensive alternative materials like pearl millet husk, date pits, sawdust, buffing dust of leather industries, coir pith, crude oil, residue, tropical grass, olive stone, apricot stone, almond shell, pine bark, wool waste, coconut shell, etc. Indigo carmine (IC) is a water-soluble derivative of the famous indigo disulfonate which has great applications in the textile industry [1]. It has also been used as additive in pharmaceutical tablets and as coloring agent in confectionery, food, beverages, and cosmetics. It also serves as a diagnostic aid, as oxidation-reduction indicator in analytical tests, and as microstain in biology [2]. IC is an acid dye [3,4] and is therefore used to dye protein fibers, wool, and silk [5], including the use of alum as a bite in the latter case [6]. Limited studies are available on the adsorption of IC on the silk and wool, in particular with regard to dyeing and the removal of effluents from textile treatments [7]. The textile industry around the world and the growing demand for ceramic paper, printing, and plastics use a wide variety of dyes as raw materials [8]. Dyes are also used in medicine, biological strains, and plastic staining [9]. Waste from these industries, in one way or another, ends up in water, thus polluting the environment. Unlike other pollutants, coloring pollutants, especially those with benzene rings, even at low concentrations, are visible, reducing the penetration of light in water, which has a negative effect on the photosynthesis of aquatic plants [10]. Similarly, the human activities have caused great damages to the quality of our lifeline, nar water [11]. IC is also used as additive in pharmac Ical tablets and capsules and for medical diagnostic pu ses. Indeed, the dye injection for cystoscopy is a saf tecl que plant [12] for detecting compromises in the urinary trac dye, and i It is considered a highly toxic class of in touch can cause skin and eye ir tion as w permanent damage to the cornea and conju on of the Zonsu dye can also be fatal because it is in ntly carcin ic and can lead to reproduction, development neurotoxi and acute toxicity. Wastewater containing IC is rich in ior and organic content and nount d led solpe ids whose pH, temperative demand e, ana nical o United Nations vary considerably Acco g to ral Öl Educational, Scientific nd Cı nization standards and 📕 Health Lation, t IC at a concentras not acc tic mg/L able in water. This ove u aye is a n aquatic life but also ance not or the huma The treatment of this waste before disposal

is therefore avy m

aqueous solutions have been one can cite the ion exchange, electrochemical n, evaporation, solvent extraction, reverse osmosis, re chem recipitation, membrane filtration, adsorption, etc. Depena in the nature of aqueous effluents, flow rates, and metal concentrations, the industrial application of these processes is restricted by the operating costs or inefficiency of the adsorption technique. These methods differ in their effectiveness in removing the IC dye from water; they have certain disadvantages, including high investment and operating costs and the need for appropriate treatment and disposal of residual dye sludge [15].

ontial. Some treatments for the removal of

This study was carried out with the aim to optimize the initial dye concentration, pH, particle size, contact time,

adsorbent dose, agitation speed, and temperature for the IC uptake. In addition, the equilibrium adsorption data were fitted to various equations for the determination of constants related to the adsorption phenomena. Equilibrium and kinetic analysis were conducted to deter ine the factors controlling the adsorption rate, the optimiza of physical parameters in the dye recovery, and to find out possibility of using this activated carbon (AC) for the de noval. This study has given encouraging results to carry out column adsorption tests und the condiapplicable to the treatment of industrial e ents, and to t the homogeneous photodegradation of IC TiO<sub>2</sub>, ZnO, ar SnO<sub>2</sub> semiconductors is the future objective

his work

## 2. Experimental

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2.1. Determina n of zero po of AC . the pH for The zero **p** Lharge which the surf rmined using a arge is procedure similar t at describe. essewhere [16]. Two hundred solutions (0.01 M) are placed rs of in clos conical flasks; th each solution is adjusted 2 and 14 by addite of HCl or NaOH solution. betw led, and the final pH is measured Then 1 g of AC is under agitat at room temperature.  $pH_{(zpc)}$  is the after 2 point v the final A versus initial pH crosses the line ïnal pi

#### node adsorption studies

exects of the experimental parameters such as Th the ir al IC concentration, pH, adsorbent dose, and temre on the IC removal are studied in batch mode a specific period of contact time. The stock solution is prepared by dissolving the accurate amount of IC (99%, Merck) in distilled water; the other solutions are prepared by dilution. pH is adjusted with HCl or NaOH. The characteristics of IC are represented in Table 1. The IC content in the supernatant is analyzed on a Perkin Elmer UV-Visible spectrophotometer model 550S ( $\lambda_{max}$  = 610 nm). The amount of IC adsorbed on AC  $q_t$  (mg/g) is calculated from the following equation:

$$q_t = \frac{\left(C_0 - C_t\right)}{m} \times V \tag{1}$$

where  $C_0$  is the initial IC concentration,  $C_t$  the IC concentrations (mg/L) at time (t), V the volume of solution (L), and mthe mass of the AC (g). Due to the inherent bias resulting from the linearization of the isotherm and kinetic models, the nonlinear regression (root mean square error, RMSE) evaluated in Eq. (2) is used as criterion for the quality of fitting [17]:

$$RMSE = \sqrt{\frac{1}{N-2} \times \sum_{1}^{N} \left( q_{e,exp} - q_{e,cal} \right)^2}$$
(2)

where  $q_{e(exp)}$  (mg/g) is the experimental value of uptake,  $q_{e(cal)}$  the calculated value using a model (mg/g), and N the



number of observations in the experiment (the number of data points). The sum of error squares (SSE) is widely used to test the validity of each model [18]:

$$SSE = \frac{1}{N} \times \sum_{1}^{N} \left( q_{e, exp} - q_{e, cal} \right)^2$$
(3)

The chi-square statistic is given by Eq. (4):

$$\chi^2 = \sum_{1}^{N} \frac{\left(q_{e, \exp} - q_{e, cal}\right)^2}{q_{e, cal}}$$

If the data from the model are mile to the perimental ones,  $\chi^2$  is small. Conversely, if the perimetal afferent, percomes large. The small the RMSE and  $\chi^2$  reactive the better to purve fitting.

AС

## 3. Results and discussio

3.1. Characterization of t

Td pore cture of the ACs surfac ng the ASAP 2010 y the quation we alcula surface area, microomeritics ipment. icropore volume were determined by the ore area, and t-plot metho 1) The total pore volume was evaluated m the a high relative pressure near (Fig. 2). The pore size distribution was detersing the density functional theory model (Fig. 3). min The n ore volume was calculated by subtracting the micropo lume from the total volume. The parameters calcula rom the isotherm diagrams and t-plot are gathered in Taole 2.

#### 3.2. Optimization study of operating conditions

The pH plays an important role in the adsorption process and particularly on the uptake capacity. It is observed that the percentage of IC removal decreases consistently with increasing pH (Fig. 4). The pH effect on IC adsorption by AC can be



Fig. 2. Adsorption isotherm of activated carbon.





explained on the basis of pH<sub>(zpc)</sub> = 5.23 (Fig. 5). The AC surface charge is negative above pH<sub>(zpc)</sub>. So, as the pH of the solution increases, the number of positively charged sites decreases and favors the IC adsorption by electrostatic attractions.

The effect of the stirring speed in the range 100–1250 rpm on the adsorption capacity onto AC is also investigated. The optimal adsorption capacity is obtained for a speed of 400 rpm which gives the best homogeneity of the mixture

Table 2

Physicochemical characteristics of activated carbon

Specific surface area (m <sup>2</sup> /g)	Porous volume (cm <sup>3</sup> /g)
S <sub>BET</sub> : 1,250.230	V <sub>T</sub> : 0.6834
S <sub>ext</sub> : 527.372	$V_{\rm mes}: 0.6684$
S <sub>mic</sub> : 753.332	$V_{\rm mic}$ : 0.0150
Pore diameter per density	1.581
functional theory (nm)	
Particle size (mm)	1.25 < Ø < 2.5
Humidity (%)	0.737
Moisture content (%)	0.743
Apparent density (g/cm <sup>3</sup> )	0.506
Reel density (g/cm <sup>3</sup> )	1.249
Total pore volume (cm <sup>3</sup> /g)	1.176
Total porosity	0.595

60 •-IC : 60 ppm 50 40 qe (mg/g) 30 Indigo Carm 20 Acid Acid 10 3 4 Fig. 4. Effect of pH on I pH (ZPC) = 5.23 Charges 3 2 0 10 11 12 13 2 3 5 9 6 8 14 pН

Fig. 5. Determination of pH of zero point charge  $pH_{(ZPC)}$  of AC.

suspension. Therefore, a speed of 400 rpm is selected for further experiments.



#### 3.3. *A* rption isotherms

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T shape of the tool to agnose the

otherms is the first experimental ture of a specific adsorption. The

value parameters for the isotherm plots

Paranter	Optimum value		
nl	2		
article size (mm)	$1.0 < \emptyset < 2.0$		
Contact time (min)	45		
Stirring speed (trs/min)	400		
Adsorbent dose (g/L)	1		
pH <sub>(ZPC)</sub>	5.23		



Fig. 6. Effect of contact time and dye concentration on removal of IC by AC.

classification of isotherms is given by Giles et al. [19]. In our case, the isotherm of IC on AC displays *L* and *S* shapes. The initial part of the *L* curve indicates a small interaction of IC/adsorption sites at low concentrations, but when the concentration  $C_0$  in the liquid phase increases, the adsorption occurs more readily. Such behavior is due to a synergistic effect with the adsorbed IC, facilitating the uptake of additional ions as a result of attractive interactions of adsorbate-adsorbate.

Five models have been tested for the adsorption equilibrium: Langmuir (Fig. 7(a)), Freundlich, Temkin, Elovich, and Dubinin-Radushkevich (Fig. 7(b)) are used in the present study, and their applicability is compared.

## 3.3.1. Langmuir isotherm

The Langmuir isotherm model [20] is based on the assumption that maximum adsorption corresponds to a saturated monolayer of solute molecules on the adsorbent surface. The linear form of the isotherm equation is given by

$$\frac{1}{C_e} = K_L q_{\max} \times \frac{1}{q_e} - K_L$$
(5)

where  $C_e$  is the equilibrium concentration (mg/L),  $q_{max}$  the monolayer adsorption capacity (mg/g), and  $K_L$  the constructed to the free adsorption energy (L/mg).

## 3.3.2. Freundlich isotherm

The linear form of the isotherm model is received by the following equation [21]:

$$\ln q_e = \ln K_F + \frac{1}{n} \ln C_e \tag{6}$$

 $K_F$  is a constant indicative of the adsorption capacity (L/g) and *n* an empirical constant related to the advertion driving force.

#### 3.3.3. Temkin isotherm

The Temkin linearized model is given

$$q_e = \frac{RT}{b} \times \ln AC_e = B \ln A + B \ln C$$

 $R_L = \frac{1}{1+1}$ 

 $C_{a}$  is the equilibrium conce ation **ς**/L), nd b are the al gas Temkin const stant, and q R is the ai. (mg/g) the adso e theoreti barameters of capacit adsorption isoth long wit on coefficients, RMSE, SSE, and  $\chi^{2}$ , ed in Taba The small the RMSE ai and  $\chi^2$  value urve fitting. oetter

The stare of adsorption of the sessed in terms of dimensionless eparation factor of equatorium parameter:

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Reverse the type of isotherm:  $(R_L = 0)$  reverse  $(0 < R_L < 1)$  favorable,  $(R_L = 1)$  linear, and  $(R_L > 1)$  havorable.

In this study,  $R_L$  lies between 0.74 and 0.90 over the  $C_0$  20–60 mg/L).  $R_L$  is less than 1, confirming that the IC



Fig. 7. (a) Langmuir isotherm model for the adsorption of IC onto AC and (b) Dubinin-Radushkevich isotherm model for the adsorption of IC onto AC.

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	Langmuir	Freundlich	Temkin	Dubinin-Radushkevich	Elovich
40°C		1/ <i>n</i> : 0.703	B: 3.14	<i>K</i> : 11.2 × 10 <sup>-4</sup> mol <sup>2</sup> k/J <sup>2</sup>	
K <sub>L</sub>	0.0058 L/mg				$K_{E}$ : 10 <sup>-5</sup> L/mg
$q_{\rm max}$	79.49 mg/g	$K_{\rm F}: 0.759 \ {\rm mg/g}$	<i>A<sub>T</sub></i> : 0.51 L/mg	<i>q</i> <sub>max</sub> : 298.34 mg/g	9 <sub>max</sub> : 11 2/g
			$\Delta Q$ : 65.52 kJ/mol	E: 21.18 kJ/mol	
RMSE	35.188	44.236	65.236	1.1885	.123
$R^2$	0.944	0.896	0.897	0.996	37
25° C		1/ <i>n</i> : 0.926	B: 6.24	<i>K</i> : 0.0014 mol <sup>2</sup> k/J <sup>2</sup>	
K <sub>L</sub>	5.2 × 10 <sup>-3</sup> L/mg	$K_{F}$ : 0.477 mg/g	$A_T : 0.265 \text{ L/mg}$	q <sub>max</sub> : 459 mg/g	
$q_{\rm max}$	83.33 mg/g		$\Delta Q$ : 0.39 kJ/mol	<i>E</i> : 19.047 J/mo	
RMSE	7.255	45.410	41.69	338	
$R^2$	0.999	0.926	0.864	0	

(9)

10)

#### Table 4 Sorption isotherm coefficients of different models

adsorption on AC is favored in both cases with the successful applicability of Langmuir isotherm.

## 3.3.4. Dubinin-Radushkevich isotherm

The Dubinin-Radushkevich isotherm can be used to describe the adsorption on both homogenous and heter ogeneous surfaces [23]:

 $\ln q_e = \ln q_m - \beta \epsilon^2$ 

 $\sqrt{2\beta}$ 

where  $q_m$  is the Dubinin-Radushkevich monotonic capacity (mg/g),  $\beta$  a constant related to sorption energy, and the Polanyi potential which is related to requilibrium concentration as follows:

$$\varepsilon = RT \ln \left( 1 + \frac{1}{C_e} \right)$$

where *R* is the gas co (mol k is the  $\beta$  gives the mean free absolute temperature, ne const energy E of adsorptio ale c e adsorbate when er m of the s it is t d to the  $\mathbf{rf}$ d from infinity in the can be uted usin he relation: 1 (11)

The agnitude of *L* is useful for estimating the action mechanism.

It is case of E < 8 kJ/mol, physical forces may affect the adsorption. Conversely, if E is in the range of 8–16 kJ/mol, adsorption on verned by ion exchange mechanism.

## 3.3.5. Elovich isotherm

The Elovich isotherm [24] is based on the principle of the kinetic assuming that the number of adsorption sites increases exponentially with the adsorption, which implies a multilayer adsorption:

$$\ln\frac{q_e}{C_e} = \ln q_m \times K_E - \frac{q_e}{q_m}$$
(12)

wich constant at equilibrium,  $q_{\max}$ ı) is th where  $K_r$  (I (mg/g)Imum nti capacity,  $q_{e}$  (mg/g) the n, and C (g/L) the equiadsor on capacity at equ of the adsorbate. The equilibrium libriu concentratio const and the max im capacity can be calculated from the plo  $\ln(q_{e}/C_{e})$  vs.

## Isorption Kinetics

The protect study is important for the adsorption process because priority it describes the uptake rate of adsorbate but also centrols the residual time of the whole process, and two model are selected to describe the adsorption process. The pseudo-first-order equation is given by [25]

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303} \times t \tag{13}$$

While the pseudo-second-order model [26] is given by

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} \times t \tag{14}$$

where  $q_t$  (mg/g) is the amount of IC adsorbed on AC at the time t (min) and  $K_1$  (min<sup>-1</sup>) and  $K_2$  (g/mg min) are the pseudo-first-order and pseudo-second-order kinetic constants, respectively.

The Elovich equation is a kinetic equation related to the chemisorption process and is validated for systems where the surface of the adsorbent is heterogeneous; the linear form is given as follows:

$$q_t = \left(\frac{1}{\beta}\right) \ln \alpha \beta + \left(\frac{1}{\beta}\right) \ln t \tag{15}$$

where  $\alpha$  (mg/g min) is the initial adsorption rate and  $\beta$  (mg/g) the relationship between the degree of surface coverage and the activation energy involved in the chemisorption. The rate constants predict the uptakes and the corresponding correlation coefficients for AC summarized in Table 5. For the pseudo-first-order kinetic (Fig. 8(a)), the experimental data



Table 5 Kinetic and intraparticle parameters for the IC adsorption onto AC

deviate fron earity as evidenced from the low values of pplicable for the present sysand  $C_0$ strast, the constation coefficient and  $q_{e'cal}$  deter-B om the pseudo-second-order kinetic model agree m with perimental data (Fig. 8(b)). Its applicability suggests the adsorption of IC onto AC is based on chemical reaction (c orption), involving an exchange of electrons between ads sent and adsorbate. In the chemisorptions, the IC ions are attached to the adsorbent surface by chemical bond and tend to find sites that maximize their coordination number with the surface.

## 3.5. Intraparticle diffusion study

The mechanisms and kinetics of the adsorption are described by various models, which predict the breakthrough curves at different times and accuracies. Nevertheless, there are not clear criteria to decide which model is convenient for a given case:

- The involved mass transfer resistances,
- Relation type between the adsorbed amount and the diffusion coefficients,
- Definitive equilibrium equation,
- Description level and the mathematical complexity of the model,

It is well known that a performed batch experiment gives valuable data to evaluate the diffusion coefficients. Under real conditions, the mass transport resistance in the solid is larger than the external fluid film on the solid particles. The possibility of intraparticle diffusion [27] during the transportation of adsorbate from solution to the particle surface was also investigated by the intraparticle diffusion model:

$$q_t = K_{\rm in}\sqrt{t} + C \tag{16}$$

where  $K_{id}$  is the intraparticle diffusion rate constant (mg/g min<sup>1/2</sup>),  $q_i$  the amount of IC adsorbed at time *t*, and *C* (mg/g) the intercept. The plot of  $q_i$  versus  $t^{1/2}$  enables to determine both  $K_{id}$  and *C* (Fig. 9). The mechanism of adsorption is complex, but the intraparticle diffusion is important in the early stages.

The first linear part could be due to intraparticle diffusion effects whose slopes are defined as the rate parameters, characteristic of the adsorption rate in the region where the intraparticle diffusion occurs.

Initially and within a short period, it is postulated that IC ions are transported to the AC external surface through the film diffusion with a high rate.

Once the surface is saturated, the IC ions enter inside AC by intraparticle diffusion through the pores and internal surface diffusion until equilibrium is reached, and this is represented by the second straight lines.

The data collected at 25°C for an initial IC concentration (20–60 mg/L) exhibit multilinear plots (Table 5). These results indicate that two or more steps occur during the adsorption process. Therefore, some boundary layer control must be involved, and the intraparticle diffusion is not limiting step.



plication of intraparticle diffusion for the adsorption o AC.

## Table 6

of

Thermodynak, c parameters for the IC adsorption onto AC

## 3.6. Effect of temperature

The adsorption reaction of coloring molecules on a surface implies a variation of the free energy  $\Delta G^{\circ}$  (kJ/mol) (variation of energy at constant pressure) between the initial and final states which predicts the feasibility on reaction.

$$\Delta G^{\circ} = \Delta H^{\circ} - T \Delta S^{\circ}$$
(17)
The energy of Cibbs is composed two terms

The energy of Gibbs is composed wo term gies of inter enthalpy term H which expresses the e tions between the molecules and the adso nt surface ar an entropic term S which expresses the fication a arrangement of the molecules d ph ehavior adsorption of IC surface. The thermodynam d. The on AC was further investig mod namic parameters ( $\Delta G^{\circ}$ ), er halpy  $(\Delta H^{\circ})$ nd e ру (Δ are calculated using the foll aatio

$$\Delta G^{\circ} = -RT \ln K_{e} \tag{18}$$

where is the apparent am constant. The apparalpy ( $\Delta H^{\circ}$ ) of the accurption and entropy ( $\Delta S^{\circ}$ ) of ent e lated from adsorption data at difthe a prption are ca ferent g Eq. (19). The adsorption capacity nperatures u ases with aising temperature over the range of AC this range, the vaporization becomes -313 🖡 reasing problem. The insights of the adsorption a rm can be determined from the free energy ( $\Delta G^{\circ}$ ), nthal  $H^{\circ}$ ), and entropy ( $\Delta S^{\circ}$ ). In the rate law, the ture dependence appears in the rate constant, and tempe mited range, it can usually be represented by Eqs. over d (20). The thermodynamic equilibrium constant (K) was dermined by Khan and Singh [28] by plotting  $\ln(q_{\perp}/C_{\perp})$ vs.  $q_{e}$  and extrapolating to zero  $q_{e}$ . The thermodynamic parameters are determined from the following equations:

$$\ln K_e = \frac{\Delta H^{\circ}}{R} \times \frac{1}{T} - \frac{\Delta S^{\circ}}{R}$$
(19)

The plot of  $\ln K_e 1/T$  is linear, and  $\Delta H^\circ$  and  $\Delta S^\circ$  are obtained from the slope and intercept of the Van't Hoff Eq. (16), while  $\Delta G^\circ$  at various temperatures is reported in Table 6. The positive  $\Delta G^\circ$  indicates a not spontaneous process, while the positive  $\Delta H^\circ$  and  $\Delta S^\circ$  show that the IC adsorption on AC is endothermic with an increased randomness at the solid-solution interface.

The rate constant and the dependence of rate constants on temperature over a limited range can usually be represented

$T$ (K) $K_e$ $R^2$ $\Delta G^{\circ}$ (kJ/mol) $\Delta H^{\circ}$ (kJ/mol) $\Delta S^{\circ}$ (kJ/mol k) $E_a$ (kJ/mol3031.0280.999-0.07053071.2310.989-0.531028.1150.09351.0653101.3630.997-0.85123171.4970.988-1.0503 $-1.0503$ $-1.0503$							
3031.0280.999-0.07053071.2310.989-0.531028.1150.09351.0653101.3630.997-0.8512-0.531028.1150.09351.0653171.4970.988-1.0503-1.0503-1.0503-1.0503-1.0503	T (K)	K <sub>e</sub>	$R^2$	$\Delta G^{\circ}$ (kJ/mol)	$\Delta H^{\circ}$ (kJ/mol)	$\Delta S^{\circ}$ (kJ/mol k)	$E_a$ (kJ/mol)
3071.2310.989-0.531028.1150.09351.0653101.3630.997-0.85123171.4970.988-1.0503	303	1.028	0.999	-0.0705			
310     1.363     0.997     -0.8512       317     1.497     0.988     -1.0503	307	1.231	0.989	-0.5310	28.115	0.093	51.065
317 1.497 0.988 -1.0503	310	1.363	0.997	-0.8512			
	317	1.497	0.988	-1.0503			

by Eq. (20). The adsorption capacity of AC increases with raising temperature in the range 299-313 K.

$$\ln K_2 = \ln A - \frac{E_a}{RT}$$
(20)

A is the pre-exponential factor,  $E_a$  the activation energy, and  $K_2$  (g/mg min) the pseudo-second-order kinetic constant at different temperatures.  $E_a$  is obtained by plotting  $\ln K_2$ against 1/T. All the calculated thermodynamic parameters are presented in Table 6.

## 3.7. Comparative study of the adsorption capacity of IC by the different adsorbents

It is instructive for a comparative purpose to report the values of the adsorption capacity of some adsorbents available in the literature (Table 7). One can see that the IC adsorption observed in this work is well positioned with respect to other researches. For our study, the maximum adsorption capacity was found to be 79.49 mg/g at 25°C and

Table 7

Adsorption capacities of IC by various adsorbents

Adsorbant	$q_{\rm max}  ({\rm mg/g})$	References
Activated carbon	298.34	This sty
Activated carbon-based KOH	13.40	[29]
Silk	18.38	[33]
Calcined (Zn/Al + Fe) layered	488.93	
double hydroxide		
TiO <sub>2</sub> /UV/O <sub>2</sub>	14.28	[32]
Mesoporous Mg/Fe layered doub	62	3]
hydroxide nanoparticles		
Nanofiber membranes	26	[34]
Acacia nilotica (Babool) sawdust	37.91	[35]
activated carbon		
Chitosan		
Carbonaceous material m	92.8	[37]
pyroly yage slud		
Br mpe. 1	31	[7]
oporous participation activity	.11	[38]
composite nar oer membranes		
Maize cob	118.48	[39]
itin p misker Zed	72.66	[40]
e an PFM		
Aph tone activated carbon	552.55	[41]
Rice hu. h	29.28	[2]
Mesoporo. lyvinyl alcohol/SiO <sub>2</sub>	495.00	[42]
nanofiber met oranes		
Urea-treated cellulosic waste of	71.07	[43]
citrus reticulata peels		
Ni nanoscale oxides/Schoenoplectus	860.23	[44]
acutus composite		
Activated sewage sludge	60.04	[45]
Nanocomposite hydrogels	370.37	[46]

298.34 mg/g at 40°C at pH 2. The differences of dye uptake are due to the properties of each adsorbent like the structure, the functional groups, and the surface area. AC could be an attractive adsorbent for basic dyes owing to the isoelectric point  $(pH_{pzc})$ .

## 4. Conclusions

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The adsorption characteristics of IC onto affected by the initial dye concentration itial pH, orable for adsorbent dose. A pH value of 2 was  $R_{L}$  values an optimum adsorption of IC dye by AC. T other adsorption parameters indicating mo

Radushkevich and Langmuir a better fit of the equilibri adsorp gave a maximum adsorption apacity which increased up to 298 mg study has sho the A tha adsorbent for the oval of om aque pseudo-second odel gav kinetic data

 $\mathbf{v} \Delta \mathbf{G}^{\circ}$  and positive enthalpy The free e  $\Delta H^{\circ}$  in ated that the adof IC onto AC is sponnic over the studied temperature and endother taneor py  $\Delta S^{\circ}$  clearly states that the ranrange ne positive en e solid-solution interface during domne ncreased at C, indicating that some structural e IC a ntion on among the active sites of the adsornge h d the ions. The adsorption of IC ions by AC follows se econd-order kinetic model, which relies on the hat the chemisorptions may be the rate-limiting ssum IC ions are attached to the adsorbent surface by step; tł a chemical bond and tend to find sites that maxiformi heir coordination number with the surface. This study In tiny batch gave rise to encouraging result, and we wish to achieve the adsorption tests in column mode under the conditions applicable to the treatment of industrial effluents, and the present investigation showed that AC is a potentially useful adsorbent for the dyes.

Future applications of the current work:

- Contribute to the reduction of environmental pollution, which remains a major international problem.
- Create agreements between the laboratory and the textile industry.
- Switch from batch mode to column mode.
- Realization of tests on an industrial scale.
- Perform theoretical simulations of phenomena.
- Preparation of new adsorbents at low economic cost.
- Elimination of pollutants by solar photodegradation.

Using the homogeneous photodegradation of IC on SnO<sub>2</sub> semiconductor is the future objective of this work. Preliminary tests were satisfactory; the experiments are currently under way and will be reported very soon.

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