



## Efficient removal of copper and lead from aqueous solution by magnetic biochar: Magnetization, adsorption, separation, and desorption

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### ABSTRACT

Efficient removal of heavy-metal ions from water is of great importance for addressing the issue of environmental pollution. In this work, a novel magnetic biochar was fabricated by loading  $\text{Fe}_3\text{O}_4$  on straw-oriented biochar ( $\text{Fe}_3\text{O}_4$ @BIO) through co-precipitation method. The preparation conditions were optimized, and the best  $\text{Fe}_3\text{O}_4$ @BIO synthesis was at BIO/ $\text{Fe}_3\text{O}_4$  weight ratio of 5:1 to 3:1. The synthesis led to higher surface area and higher adsorption capacity for  $\text{Cu}^{2+}$  (143.2 mg/g) but relatively low capacity for  $\text{Pb}^{2+}$  (463.8 mg/g) as compared with non-magnetic biochar (56.1 and 665.4 mg/g, respectively). This means that different mechanisms dominated the adsorption processes for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$ . After four times of regeneration and reuse, the adsorption capacity retained 60%–70% of the level in the initial situation. Overall, our magnetic biochars are considered suitable for use in wastewater treatment processes because of their excellent heavy-metal adsorption ability and easy recovery after use.

*Keywords:* Magnetic biochar; Adsorption; Copper(II); Lead(II)

### 1. Introduction

Heavy-metal ions  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  are common pollutants in chemical, metallurgy, mining, electroplate, coking, and other related industries. When they are present or discharged at certain concentrations, they can be injurious and toxic to aquatic ecosystems since they resist decomposition and because they can accumulate in organisms; hence, their presence in water is a critical general health issue. Exposure to copper ions can cause lethargy, DNA damage, gastrointestinal bleeding, and hypertension [1], while lead exposure can result in anemia, chills, dysfunction, and diarrhea of kidney [2]. Their concentration in industrial wastewater can reach thousands of milligrams per liter. Thus, the separation and recycling of these pollutants has progressed into a critical issue.

Several methods have already been developed recently to remove heavy metals from solutions, such as chemical

precipitation, ion exchange, filtration, electroplating, reverse osmosis, and adsorption [3]. Among these technologies, adsorption is considered as a reliable modern technology. It is preferred by industries because of its easy operation, high efficiency, and low cost of production. A series of materials such as activated carbon, fly ash, zeolites, and montmorillonite have been reported to have excellent properties for the removal of heavy metals from solutions [4–6]. It is certain that the powdered form of adsorbents are more efficient at pollutant removal than the granular form. Activated carbon is considered as the best adsorbent because it provides large surface area and hence high adsorption capacity [7]. But in recent studies, biochar that is similar to activated carbon and produced via thermal decomposition of biomass rich in carbon constituents, both of which belong to black carbon, has been shown to have better characteristics than activated carbon for metal removal [8].

Due to the presence of the rich porous structure and various functional groups, biochar exhibited a great poten-

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tial for heavy metals adsorption in wastewater. Commonly the feedstock materials for biochar in studies are agricultural wastes including sawdust, peanut shells, bagasse, rice straw, fruit peel and so on [8]. As the research into biochar has been great active in recent years, various kind of raw materials have been applied and studied to remove heavy metals such as daily manure, marine macro-algae and wastewater sludge [9–11]. But the output of these raw materials' are lower than agricultural wastes, and manufactured biochars' adsorption characteristic are also not as well as those biochar derived from agricultural wastes [8]. Moreover, many investigations of biochar and magnetic biochars have been biased toward the study of organic materials and anionic heavy metals in order to emphasize the adsorption ability of biochars, whereas studies related to cationic heavy metals adsorption are lacking [10]. It is necessary to found the biochar with abundant raw materials source and excellent adsorption capacity for heavy metals.

In addition, powdered biochar adsorbents can be difficult to separate from wastewater; therefore, they have been traditionally released with the process sludge into the environment, resulting in secondary pollution or another treatment process cost. Thus, magnetic separation is a suitable technology for the separation of adsorbents from wastewater. It is well known that  $\text{Fe}_3\text{O}_4$  process rapidly magnetic responsibility when the external magnetic field is applied. Moreover, the adsorption properties of biochar such as adsorption capability, surface area, zeta potential, and kinetic and thermodynamic characteristics could be improved by loading magnetic materials [2,12,13], whereas some studies also find that the magnetization of the biochar by  $\text{Fe}_3\text{O}_4$  partially reduce its adsorption efficiency due to the biochar's surface pores becoming plugged with iron oxide particles [2]. Generally, several previous studies have been conducted for the manufacture of magnetic biochar and the adsorption properties for heavy metals, but these studies mainly focus on the novelty of the material, the process of magnetization, and the separation efficiency of the adsorbents rather than the mechanism of the adsorption process, adsorption capacity and method optimization.

Thus, in order to provide an adsorbent with adequate raw materials and excellent sorption capability for heavy metals eliminating, a biochar derived from straw was selected for magnetic biochar ( $\text{Fe}_3\text{O}_4$ @BIO) synthesis by in situ co-precipitation in this paper. The sorption of  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  on biochar and  $\text{Fe}_3\text{O}_4$ @BIO composites were measured, and the adsorption capability of  $\text{Fe}_3\text{O}_4$ @BIO were optimized. The adsorption kinetics, thermodynamics, and the effect of some environmental factors are discussed. In addition, the adsorption mechanism was investigated by means of batch experiments, adsorption model, and characterization techniques.

## 2. Material and methods

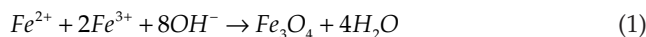
### 2.1. Chemicals and material

All chemicals used in this study were analytically pure, including  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$ ,  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ ,  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$ ,  $\text{Pb}(\text{NO}_3)_2$ ,  $\text{NaCl}$ ,  $\text{KCl}$ ,  $\text{MgCl}_2$ ,  $\text{CaCl}_2$ ,  $\text{HNO}_3$ , and  $\text{NaOH}$ . The stock solution of  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  (1000 mg/L) were prepared by dissolving  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$ ,  $\text{Pb}(\text{NO}_3)_2$  in dis-

tilled water (DW). A straw-oriented gasification biochar (BIO) was selected as the adsorbent. In brief, the agricultural straw purchased from the company of Yuzhonggao (Henan, China) was air-dried in a fume cupboard, crushed by a pulverizer, pyrolyzed at approximately  $550^\circ\text{C}$  in a kiln for 2 h, and then ground until they pass through a 100-mesh sieve. The BIO was stored in a drying oven for subsequent study.

### 2.2. Fabrication of magnetic biochar

The preparation of magnetic biochar ( $\text{Fe}_3\text{O}_4$ @BIO) was similar to that in a previous study [10]. First, a certain mass of BIO was dispersed in 100 mL of DW and stirred by a magnetic stirrer. Second, 50 mL of  $\text{FeSO}_4$  at a certain concentration was added to the above solution, and then 50 mL of  $\text{FeCl}_3$  solution at a certain concentration was added. After thorough stirring for 15 min, 10 M  $\text{NaOH}$  solution was added dropwise to the  $\text{BIO}/\text{Fe}^{2+}/\text{Fe}^{3+}$  solution until the pH reached 10–11. The mixture was allowed to react for 8 h at room temperature, and the obtained  $\text{Fe}_3\text{O}_4$ @BIO was magnetically separated and washed with DW several times to remove the impurities. Finally, the solid sample was freeze-dried for 48 h. The concentration of  $\text{FeSO}_4$  and  $\text{FeCl}_3$  were calculated previously to synthesize different mass ration of  $\text{Fe}_3\text{O}_4$  loaded onto BIO according to Eq. (1), the mass ration of  $\text{BIO}:\text{Fe}_3\text{O}_4$  were ranging from 7:1 to 1:3. The adsorption capacity of these  $\text{Fe}_3\text{O}_4$ @BIO powders for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  were measured, respectively.



### 2.3. Characterization of the surface properties

The specific surface area was determined with the Brunauer–Emmett–Teller (BET) equation with multi point adsorption isotherms of  $\text{N}_2$  at 77 K (Micro meritics ASAP 2020). The surface morphology was analyzed by scanning electron microscopy (SEM-EDS; S-4800/EX-350, Hitachi, Japan). The functional groups on the powder sample surface were recorded using Fourier transform infrared spectra (FTIR) over the spectral range of  $4000\text{--}400\text{ cm}^{-1}$  at a resolution of  $4\text{ cm}^{-1}$  by using pressed KBr discs. (Affinity-1, Shimadzu, Japan). The crystallographic structures were analyzed by power X-ray diffraction (XRD, X-Pert Pro MPD, Panalytical, Holland). The chemical compositions were confirmed by X-ray photo electron spectrometry (XPS, ESCSLAB 250Xi, Thermo Fisher, USA).

### 2.4. Batch sorption experiments

In batch experiments, a certain amount of BIO or  $\text{Fe}_3\text{O}_4$ @BIO was add to 50 mL polyethylene centrifuge tubes and mixed with a certain volume of  $\text{Cu}^{2+}$  or  $\text{Pb}^{2+}$  solution. The solid/liquid ratios of  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  solutions were fixed at 2:1 and 1:2, respectively. The adsorption isotherms were obtained by using the adsorption experimental results of the different  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  solutions with concentrations ranging from 100 to 1000 mg/L. The adsorption kinetics was examined at reaction time intervals ranging from 0.5 to 48 h with 500 mg/L heavy

metal solution at free pH. The effect of pH on adsorption capacity was studied by adjusting pH values from 2 to 7 by using diluted  $\text{HNO}_3$  and  $\text{NaOH}$  solution. The cations  $\text{K}^+$ ,  $\text{Ca}^{2+}$ ,  $\text{Na}^+$ , and  $\text{Mg}^{2+}$  at concentrations of 0–50 mmol/L were used to study the effect of competitive adsorption. Except of adsorption kinetics other adsorption tests were conducted 48 h. After a predetermined time of shaking at 180 rpm in a shaker, the supernatant was filtered through a 0.45  $\mu\text{m}$  membrane, treated with 1 mol/L of nitric acid, and stored at 4°C until analysis. The residual concentration of metals remaining in adsorption solution was analyzed by an atomic absorption spectrophotometer (ICE3500, Thermo Fisher, USA) or by inductively coupled plasma mass spectrometry.

The adsorption capacity ( $Q_e$ , mg/g) of BIO or  $\text{Fe}_3\text{O}_4$ @BIO for heavy-metal ions was calculated by the following equation:

$$Q_e = \frac{(C_0 - C_e) \times V}{m} \quad (2)$$

where  $C_0$  and  $C_e$  (mg/L) are, respectively, the initial and equilibrium concentrations of the heavy-metal ions.  $V$  (L) is the volume of the adsorption solution, and  $m$  (g) is the mass of adsorbent.

### 3. Results and discussion

#### 3.1. Characterization of BIO before and after magnetization

##### 3.1.1. Optimum $\text{Fe}_3\text{O}_4$ loading for magnetization

Fig. 1a shows the adsorption capacity and recovery efficiency of BIO and  $\text{Fe}_3\text{O}_4$ @BIO for  $\text{Cu}^{2+}$ . It is observed that with increasing BIO/ $\text{Fe}_3\text{O}_4$  mass ratio, the adsorption of  $\text{Cu}^{2+}$  on  $\text{Fe}_3\text{O}_4$ @BIO increased up to 170.3 mg/g at a mass ratio of 5:1 and then decreased with further increase of the BIO/ $\text{Fe}_3\text{O}_4$  mass ratio. As for  $\text{Pb}^{2+}$  (Fig. 1b), the highest adsorption capacity (674 mg/g) was observed as the BIO/ $\text{Fe}_3\text{O}_4$  weight ratio was fixed at 1:0; it was always decreasing as when the loading had more  $\text{Fe}_3\text{O}_4$ . In addition,

the high proportion of  $\text{Fe}_3\text{O}_4$  led to high recovery efficiency and large BET surface area, and the recovery efficiency reached 87.5% at a mass ratio of 5:1. Comparison with BIO showed that the BET surface area of  $\text{Fe}_3\text{O}_4$ @BIO reached 124.3  $\text{m}^2/\text{g}$  at the lowest BIO/ $\text{Fe}_3\text{O}_4$  ratio in this study. The synthetic  $\text{Fe}_3\text{O}_4$  through co-precipitation was almost nanoscale; it could cover the surface of BIO and could react with functional groups such as C=O, C–O, C–H, and O–H, as can be concluded from FTIR analysis (Fig. 3). This resulted in a change in  $\text{Fe}_3\text{O}_4$ @BIO adsorption capability for metal ions. So, it is essential to determine the optimum BIO/ $\text{Fe}_3\text{O}_4$  mass ratio that maximizes the separation efficiency of  $\text{Fe}_3\text{O}_4$ @BIO and the adsorption of copper without sacrificing much of its adsorption capacity for lead.

In order to achieve the high adsorption capacity and recovery efficiency, the optimum BIO/ $\text{Fe}_3\text{O}_4$  mass ratio was fixed at 5:1 to 3:1 (Fig. 1). In the subsequent study, the adsorbent was synthesized at a ratio of 3:1 because the  $\text{Fe}_3\text{O}_4$ @BIO composite can maintain the magnetic properties and adsorption capability during multiple reuses.

#### 3.1.2. Surface characterization

The surface morphology of BIO and  $\text{Fe}_3\text{O}_4$ @BIO were characterized by SEM-EDS. Fig. 2a shows that BIO exhibits a highly porous structure with a relatively smooth surface as compared with  $\text{Fe}_3\text{O}_4$ @BIO. The wrinkled surface and richer porous structure of the BIO allows the  $\text{Fe}_3\text{O}_4$  to be more easily loaded onto or into the BIO. After magnetization, the  $\text{Fe}_3\text{O}_4$  particles appeared on the surface of BIO, which exhibited a relatively rough surface as compared with the BIO. The appearance of the signal of Fe indicates that  $\text{Fe}_3\text{O}_4$ @BIO was successfully prepared (Fig. 2d).

The FTIR spectra of BIO,  $\text{Fe}_3\text{O}_4$ , and  $\text{Fe}_3\text{O}_4$ @BIO composite are presented in Fig. 3a. The peak at 3281–3644  $\text{cm}^{-1}$  is assigned to the O–H stretching vibration, the peak at 1430  $\text{cm}^{-1}$  is matched to the C=O stretching vibration, and the peaks within 1038 and 876  $\text{cm}^{-1}$  are ascribed to the C–O stretching vibration and C–H plane deformation vibra-

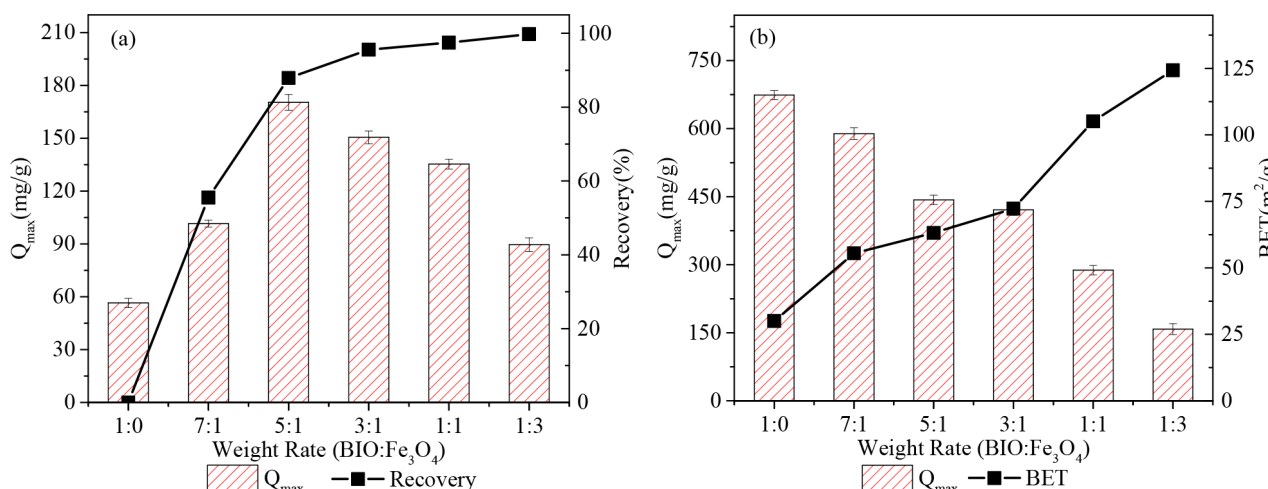


Fig. 1. The adsorption of BIO@ $\text{Fe}_3\text{O}_4$  for  $\text{Cu}^{2+}$  (a) and  $\text{Pb}^{2+}$  (b) and the recovery efficiency (a) and BET (b) of BIO@ $\text{Fe}_3\text{O}_4$  composite at different weight rate.

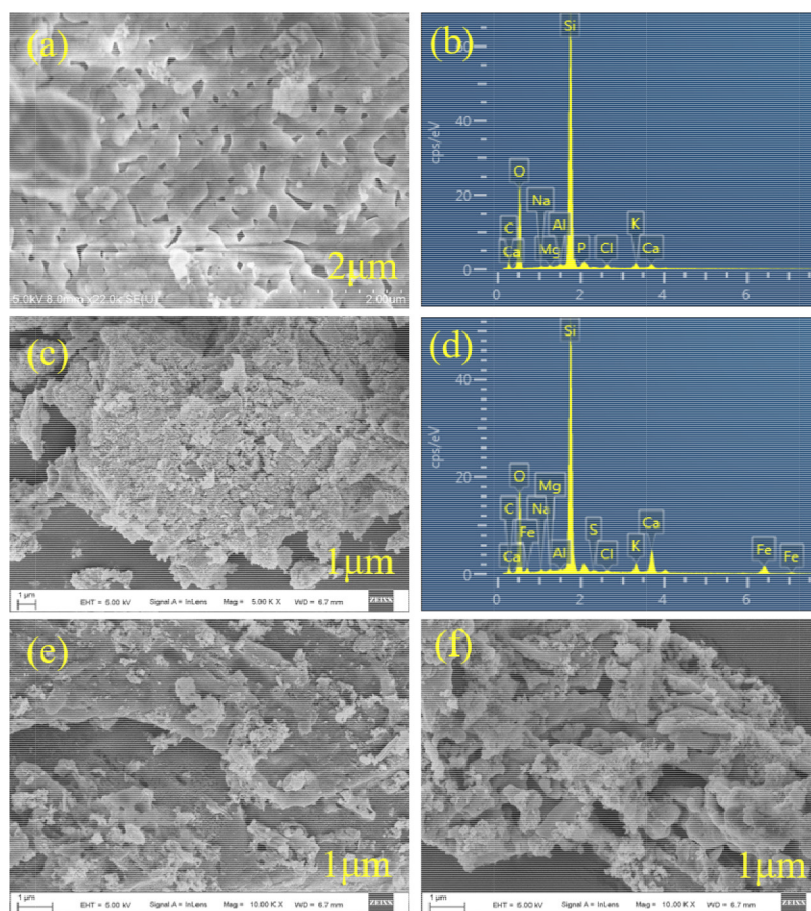


Fig. 2. The SEM-EDS of BIO (a and b) and BIO@Fe<sub>3</sub>O<sub>4</sub> (c and d) before adsorption test, and the SEM of BIO@Fe<sub>3</sub>O<sub>4</sub>-Cu (e) and BIO@Fe<sub>3</sub>O<sub>4</sub>-Pb (f) after adsorption test.

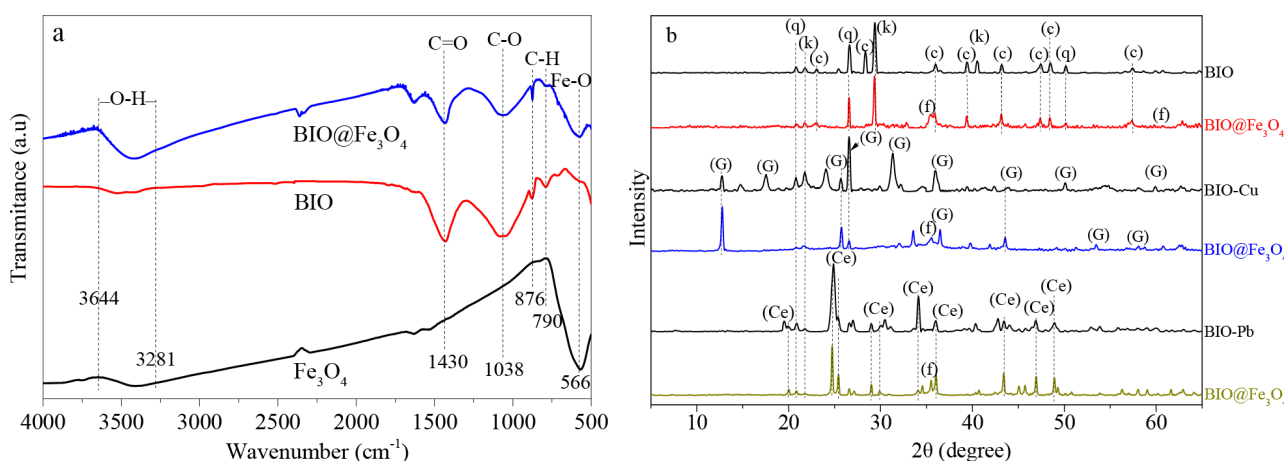


Fig. 3. The FTIR spectra of Fe<sub>3</sub>O<sub>4</sub>, BIO and BIO@Fe<sub>3</sub>O<sub>4</sub> (a) and XRD patterns of BIO and BIO@Fe<sub>3</sub>O<sub>4</sub> before and after adsorption test (b). (q): SiO<sub>2</sub>, (k): KCl, (c): CaCO<sub>3</sub>, (f): Fe<sub>3</sub>O<sub>4</sub>, (Ce): PbCO<sub>3</sub>, (G): Gerhardtite

tion, respectively [14,15]. The band at 566 cm<sup>-1</sup> of Fe<sub>3</sub>O<sub>4</sub> is attributed to the stretching vibration of Fe-O [10], which is also observed in the Fe<sub>3</sub>O<sub>4</sub>@BIO composite and similar with other related study [16]. Comparison with BIO revealed that the bonds of Fe<sub>3</sub>O<sub>4</sub>@BIO appeared at the same wavenumber; this shows that the basic surface characteristics

of the BIO remains unchanged largely after magnetization by Fe<sub>3</sub>O<sub>4</sub>.

XRD patterns for BIO and Fe<sub>3</sub>O<sub>4</sub>@BIO are presented in Fig. 3b. The result indicates that the solid samples were dominated by calcite and quartz. For Fe<sub>3</sub>O<sub>4</sub>@BIO, it was observed new peaks at 2θ = 35.7°, 43.0°, 56.8°, 62.5°

( $\text{Fe}_3\text{O}_4$ ), and the shape of  $\text{Fe}_3\text{O}_4$ @BIO pattern did not change noticeably as compared with BIO. Similarly, XPS analysis showed that, the element Fe was successfully loaded onto the surface of BIO (Fig. 4). The Fe 2p peak further demonstrates that iron oxides in the composite are  $\text{Fe}_3\text{O}_4$  rather than  $\text{Fe}_2\text{O}_3$  [17], consistent with the result of XRD analysis.

### 3.2. Adsorption study

#### 3.2.1. Adsorption kinetics

The effects of reaction time on adsorption capacity for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  of BIO and  $\text{Fe}_3\text{O}_4$ @BIO are shown in Fig. 5. There was no obvious difference between BIO and  $\text{Fe}_3\text{O}_4$ @BIO for  $\text{Pb}^{2+}$  in terms of achieving adsorption equilibrium

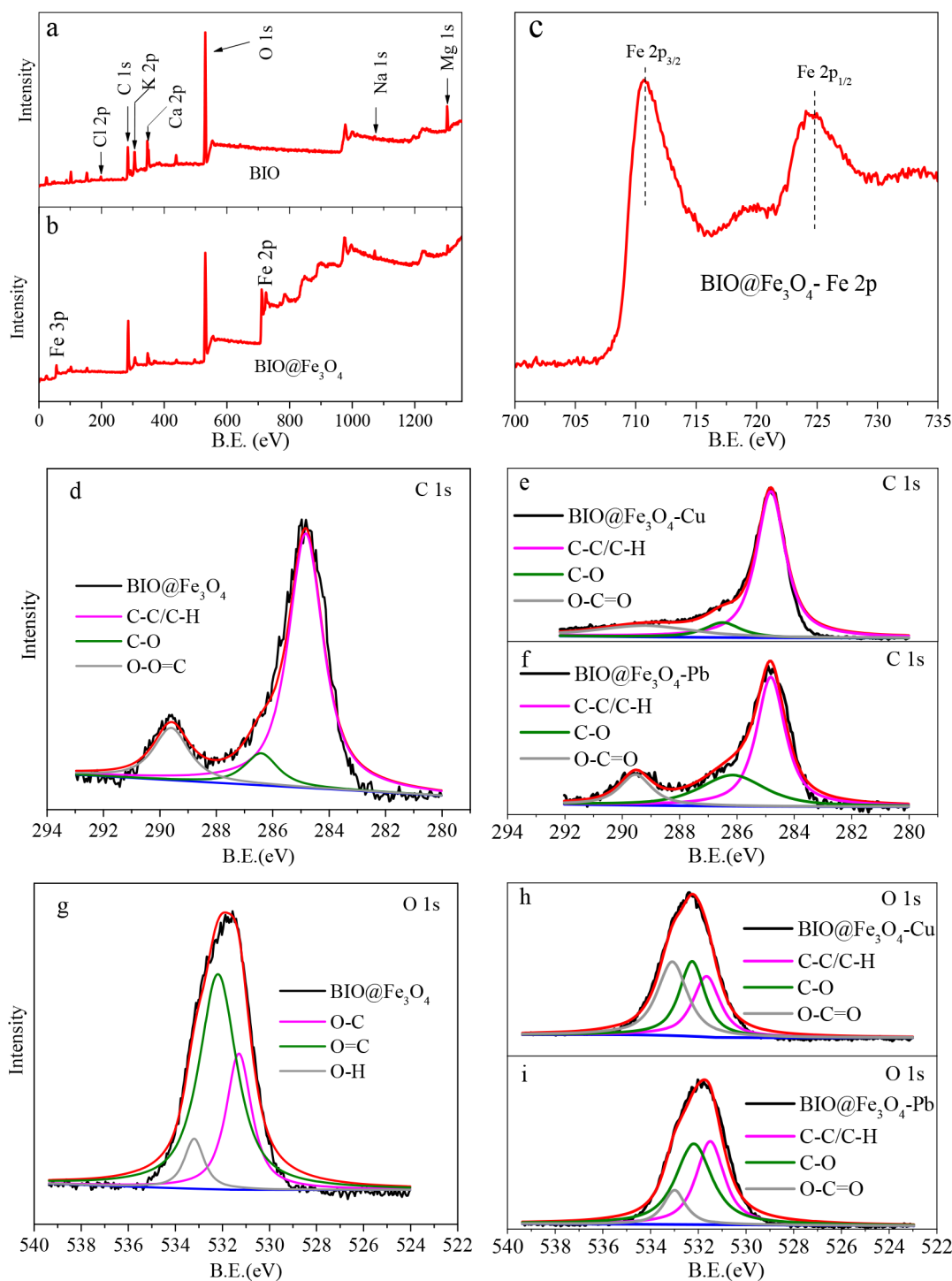


Fig. 4. The XPS of wide scan of BIO (a) and  $\text{BIO@Fe}_3\text{O}_4$  (b), Fe 2p spectrum of  $\text{BIO@Fe}_3\text{O}_4$  (c) composite, and C 1s and O 1s of  $\text{BIO@Fe}_3\text{O}_4$  before (d and g) and after adsorption Cu (e and h) and Pb (f and i), respectively.

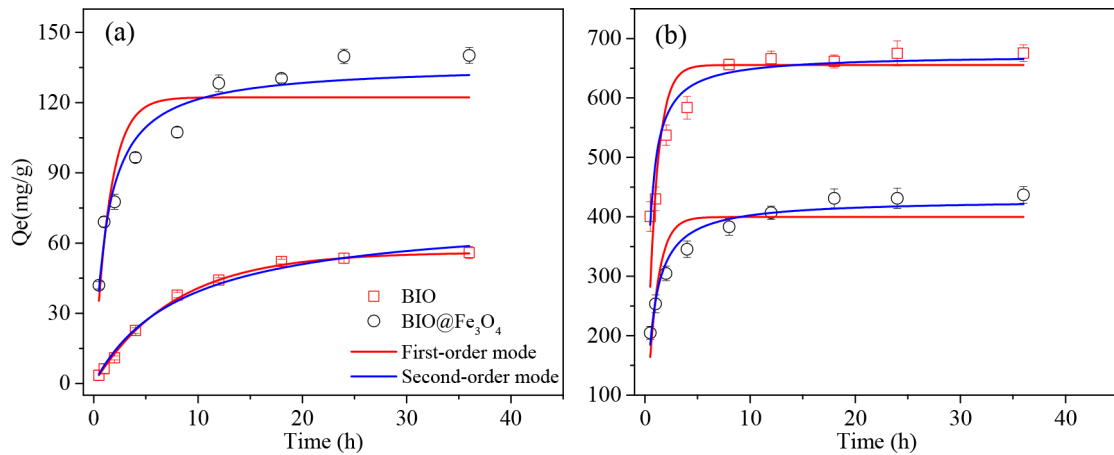


Fig. 5. Adsorption kinetics for  $\text{Cu}^{2+}$  (a) and  $\text{Pb}^{2+}$  (b) at  $25^\circ\text{C}$ .

(approximately 9 h), but for  $\text{Cu}^{2+}$  the  $\text{Fe}_3\text{O}_4$  loading on BIO surface could shorten the equilibrium time from 18 to 12 h. It was observed that the adsorption capacity of  $\text{Fe}_3\text{O}_4\text{@BIO}$  for  $\text{Cu}^{2+}$  (122.2 mg/g) was almost two times higher than that of BIO (56.1 mg/g), whereas that for  $\text{Pb}^{2+}$  (435.6 mg/g) was lower than that of BIO (665.4 mg/g). In order to explore the mechanism of the adsorption process, the experimental data were analyzed by the pseudo-first-order [Eq. (1)] and the pseudo-second-order [Eq. (2)] models:

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303} \cdot t \quad (3)$$

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad (4)$$

where  $q_t$  and  $q_e$  (mg/g) are adsorption capacity at time  $t$  and at equilibrium, respectively;  $k_1$  and  $k_2$  ( $\text{h}^{-1}$ ) are the pseudo-first-order and pseudo-second-order adsorption rate constants, respectively. The fitted plots are shown in Fig. 5, and the parameters of these two models are summarized in Table 1. It can be easily concluded from these results that all of the correlation coefficients ( $R^2$ ) of pseudo-second-order model are better than those of the pseudo-first-order model. In addition, the calculated value of  $q_e$  in the pseudo-second-order model was closer to the real value, indicating that electron transfer and the chemical adsorption are the rate-limiting step in the adsorption process [16].

Table 1  
Best-fit model parameters for the adsorption kinetics

Metal	Adsorbent	First-order			Second-order		
		$Q_{max}$ , mg/g	$k_1$	$R^2$	$Q_{max}$ , mg/g	$k_2$	$R^2$
Cu	BIO	56.1	0.13	0.99	60.5	0.0016	0.99
	$\text{BIO@Fe}_3\text{O}_4$	122.2	0.68	0.89	136.2	0.006	0.96
Pb	BIO	665.4	1.12	0.80	672.3	0.004	0.85
	$\text{BIO@Fe}_3\text{O}_4$	435.6	1.06	0.82	428.9	0.0035	0.96

### 3.2.2. Adsorption isotherms

The relationship between initial concentrations of the adsorbate and the adsorption capacity at a given temperature can be described by the adsorption isotherms (Fig. 6). This analysis can provide further information about the adsorption process and the optimum adsorption system for efficient separation of heavy metals from solution. Two isotherm models were used to fit the isotherm data: Langmuir [Eq. (3)] and Freundlich [Eq. (4)]. The Langmuir isotherm assumes that the adsorption occurs at a mono layer, with no interaction between the adsorbed molecule [18,19]. The Freundlich isotherm assumes multilayer and non-ideal adsorption on a heterogeneous surface with a non-uniform distribution of adsorption activation energy [19]. These non-linear equations can be described as follows:

$$Q_e = \frac{K_L Q_{max} C_e}{1 + K_L C_e} \quad (5)$$

$$Q_e = K_F C_e^m \quad (6)$$

where  $K_L$  (L/mg) is the Langmuir equilibrium adsorption constant related to the affinity of binding sites, and  $K_F$  ( $\text{mg}^{(1-m)}\text{L}^n/\text{g}$ ) is the Freundlich affinity coefficient, respectively.  $Q_{max}$  (mg/g) is the maximum adsorption capacity of the sorbent,  $C_e$  (mg/L) is the equilibrium concentration of the sorbate,  $m$  is the Freundlich linearity constant, and  $Q_e$  is the adsorption capacity at equilibrium (mg/g). The Langmuir and Freundlich parameters are listed in Table

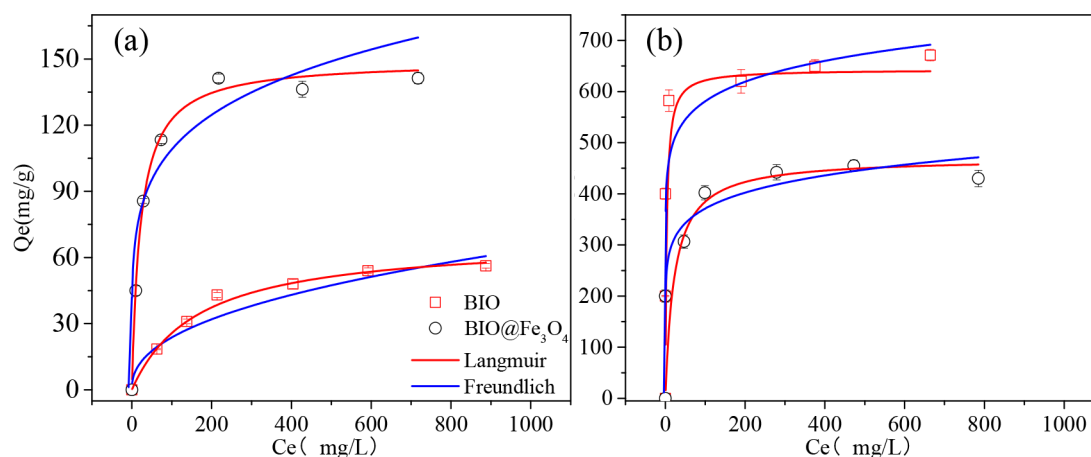


Fig. 6. Adsorption isotherms for  $\text{Cu}^{2+}$  (a) and  $\text{Pb}^{2+}$  (b) at 25 °C.

Table 2  
Best-fit model parameters for the adsorption isotherms

Metal	Adsorbent	Langmuir			Freundlich		
		$Q_{max}$ , mg/g	$K_L$	$R^2$	$K_f$	$m$	$R^2$
Cu	BIO	66.4	0.006	0.99	3.2836	0.4294	0.93
	$\text{BIO@Fe}_3\text{O}_4$	149.2	0.046	0.99	44.5745	0.1941	0.78
Pb	BIO	642.9	0.293	0.95	380.34	0.0919	0.93
	$\text{BIO@Fe}_3\text{O}_4$	470.2	0.045	0.90	217.63	0.1159	0.76

2.  $Q_{max}$  of  $\text{Fe}_3\text{O}_4\text{@BIO}$  for  $\text{Cu}^{2+}$  was 149.2 mg/g, which was approximately 2.2 times higher than that of BIO;  $Q_{max}$  of  $\text{BIO@Fe}_3\text{O}_4$  for  $\text{Pb}^{2+}$  decreased by 26.9% relative to that of BIO. The reason for this opposite result may be attributed to different adsorption mechanisms for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$ . The bound of  $\text{Pb}^{2+}$  may be dominated by both the physisorption and chemisorption processes such as surface co-precipitation and ion exchange. But for  $\text{Cu}^{2+}$ , the adsorption process may be controlled by the physical adsorption or electrostatic interaction and shared with chemisorption. In addition, all  $R^2$  values of the Langmuir are higher than Freundlich, as shown in Table 2, suggesting that the sorption of  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  on both BIO and  $\text{Fe}_3\text{O}_4\text{@BIO}$  is dominated by mono layer adsorption [16].

### 3.2.3. Effect of initial pH

It is well known that pH plays an important role in the adsorption process because it affects the degree of ionization and speciation of the heavy metals, as well as the charges and states of the functional groups of the adsorbent. As the magnetic particles consist of iron oxides, a heavily acidic condition can induce the leaching of iron ions into the wastewater, thus possibly having a negative effect on magnetic separation. Fig. 7 shows the effect of the initial pH on the sorption capability and recovery efficiency of  $\text{Fe}_3\text{O}_4\text{@BIO}$ . With increasing pH value from 2 to 7, the adsorbent capability of  $\text{Fe}_3\text{O}_4\text{@BIO}$  increased from 48.4 to 226.1 mg/g for  $\text{Cu}^{2+}$  and from 150.6 to 616.1 mg/g for  $\text{Pb}^{2+}$ . In addition, the recovery efficiency of  $\text{Fe}_3\text{O}_4\text{@}$

BIO composite was enhanced with the increase in the pH value. At the lowest pH, the adsorbent recovery efficiencies of the two adsorption systems were below 50%; when the pH rose to  $\geq 5$ , almost 90% of the  $\text{Fe}_3\text{O}_4\text{@BIO}$  could be recovered.

Usually at relatively low pH, copper ions and lead ions commonly exist as bivalent ions, and  $\text{H}^+$  at high concentration can compete with them for adsorption sites. A high  $\text{H}^+$  activity promotes protonation of the surface groups on the adsorbent and thus repulsion of the heavy-metal ions [19], resulting in a decline of adsorption capability. Along with increase in pH, the decrease in  $\text{H}^+$  activity could reduce the competitive adsorption, resulting in an increase in adsorption capacity [19]. When the pH was close to 7 under the study conditions, the heavy metals could react with  $\text{OH}^-$  to form precipitations promoting the removal of  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  from solutions.

### 3.2.4. Effect of coexisting ions

In addition to pH, coexisting of ions such as  $\text{Na}^+$ ,  $\text{K}^+$ ,  $\text{Ca}^{2+}$ , and  $\text{Mg}^{2+}$ , which are abundant in the natural environment, can also compete with heavy metals for adsorption sites and thus have an effect on adsorbent capability. In Fig. 8, the adsorption capacity of  $\text{Fe}_3\text{O}_4\text{@BIO}$  for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  in the presence of other cations is lower than that of blank. When these four cations were added, the adsorption capacity was markedly inhibited in the following order:  $\text{Ca}^{2+} > \text{Mg}^{2+} > \text{K}^+ > \text{Na}^+$ . The adsorption capacity decreased with increasing concentration of

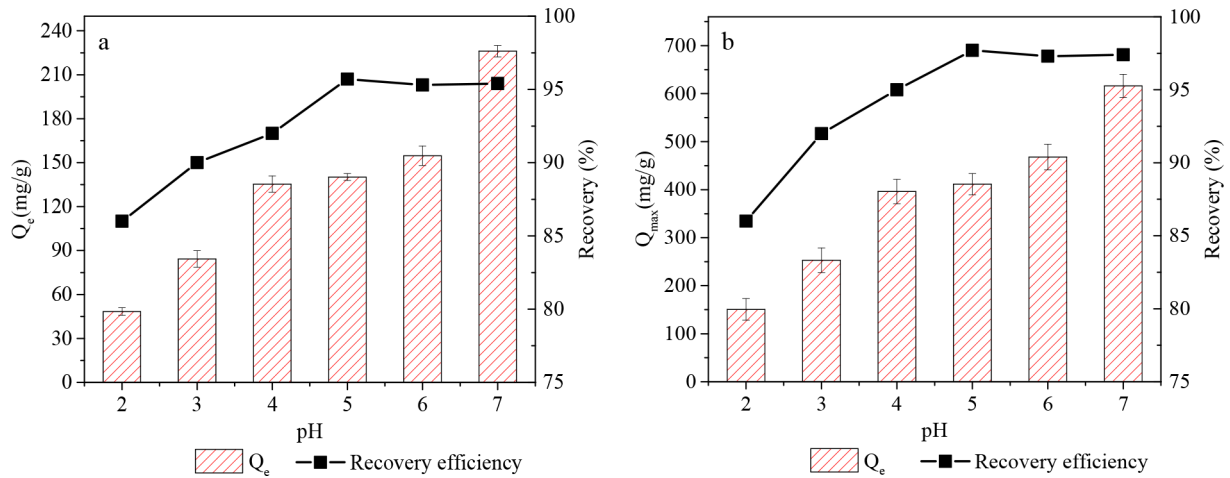


Fig. 7. The effect of pH on  $\text{Fe}_3\text{O}_4$ @BIO sorption capacity ( $Q_e$ ) and its recovery efficiency for  $\text{Cu}^{2+}$  (a) and  $\text{Pb}^{2+}$  (b).

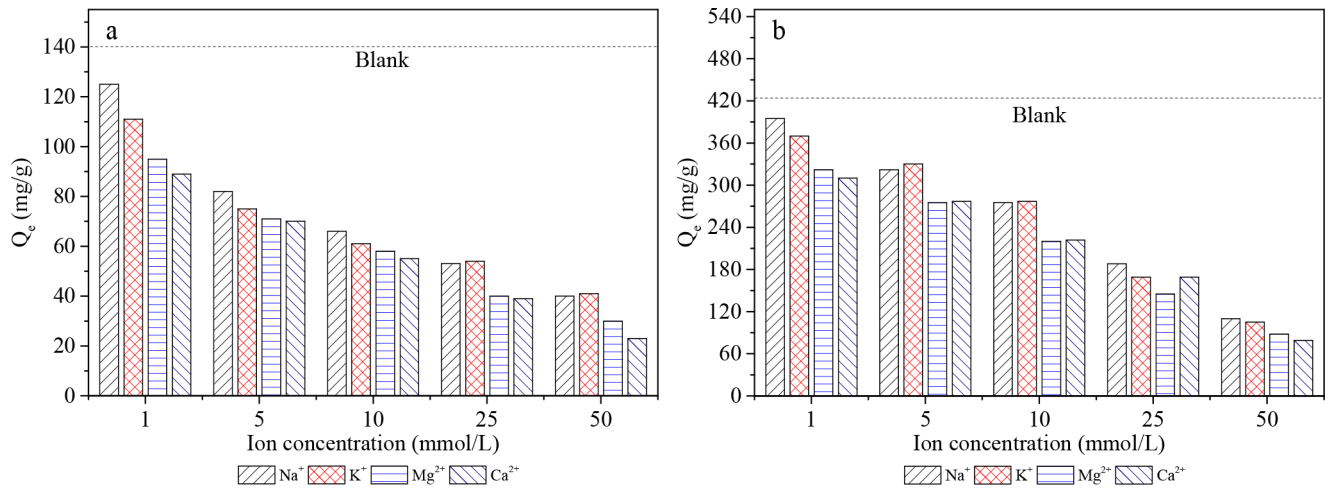


Fig. 8. The effect of ion strength on  $\text{Fe}_3\text{O}_4$ @BIO sorption capacity for  $\text{Cu}^{2+}$  (a) and  $\text{Pb}^{2+}$  (b).

coexisting cation. Cation exchange and competition can explain these results, but the internal mechanism remains unclear [20]. In some studies, the ionic radii were considered as one of the reasons for competing adsorption [21,22]. The hydrated cation represents its effective form in the aqueous solution, and it has greater size than the ionic radius. As shown in Table 3 [23,24], the hydrated

radii of related cations decrease in the following order:  $\text{Mg}^{2+} > \text{Ca}^{2+} > \text{Na}^+ > \text{K}^+$ , indicating that the adsorption capacity and the hydrated radii of the cations are in the reverse sequence under the same charge number conditions. However, another study pointed out that the adsorption capacity is affected by the ion hydration and the charge number of the ions. Therefore, the adsorption affinity of the coexisting cation ions could be compared through the following equation, which is similar to Coulomb's electrostatic law:

$$F = k \frac{|q_1 q_2|}{r^2} \quad (7)$$

where  $k$  ( $\text{N}\cdot\text{m}^2/\text{C}^2$ ) is a constant;  $q_1$  (C) and  $q_2$  are the charges of the adsorbent and ion, respectively; and  $r$  (m) is the distance between the charges. The higher was the  $F$  value of the coexisting ions, the stronger was the binding affinity and the more obvious was the inhibitory effect on the adsorption of  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  [16]. According to the calculation, the adsorption affinity decreases in the following order:  $F_{\text{Ca}^{2+}} > F_{\text{Mg}^{2+}} > F_{\text{K}^+} > F_{\text{Na}^+}$ , which is consistent with the experimental data in this study.

Table 3  
The bare and hydrated radii of the cations

Ion	Ion radius (nm)	Hydrated radius (nm)
$\text{H}_3\text{O}^+$	0.115	0.28
$\text{Ca}^{2+}$	0.100	0.412
$\text{Mg}^{2+}$	0.072	0.428
$\text{Na}^+$	0.117	0.358
$\text{K}^+$	0.149	0.331
$\text{Cu}^{2+}$	0.073	0.325
$\text{Pb}^{2+}$	0.132	0.401



### 3.3. Adsorption mechanism

The adsorption process of heavy-metal ions can be generally concluded as physical and chemical binding mechanisms. The morphology of the surface of  $\text{Fe}_3\text{O}_4\text{/BIO}$  changed markedly after adsorption  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$ , as shown in Figs. 2c, e, and f. Before adsorption, there are some pore structures and rough surface in  $\text{Fe}_3\text{O}_4\text{/BIO}$ , whereas, after adsorption experiment, the pore structure is blocked and disappeared completely, the surface of  $\text{Fe}_3\text{O}_4\text{/BIO}$  is becoming smooth, and the new compounds be generated with the shape of amorphous or crystalline granular, which suggest that surface co-precipitation had great contribution to the adsorption process. Through element analysis by XPS, the C 1s spectrum of  $\text{Fe}_3\text{O}_4\text{/BIO}$  was deconvoluted into three components (Fig. 4d): C–C/C–H at 284.83 eV, C–O at 286.40 eV, and O–O=C at 289.59 eV [16,19]. The O 1s spectrum was composed of three peaks for O–C, O=C, and O–H at binding energy (BEs) of 531.49, 532.18, and 532.99 eV, respectively [16,19]. The BEs of the C 1s and O 1s spectra of  $\text{Fe}_3\text{O}_4\text{/BIO}$  after adsorption  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  are compared in Table 4. Although the elements of  $\text{Fe}_3\text{O}_4\text{/BIO}$  after adsorption of  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  show the same functionalities as those of  $\text{Fe}_3\text{O}_4\text{/BIO}$ , there was a different for binding energy after adsorption. The change of the BEs values of Fe 2p was not significant, suggesting that the Fe atom does not participate in  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  chemical bonding adsorption. Whereas the BEs of C 1s and O 1s shifted, indicating that hydroxyl and carboxyl are the active position for adsorption  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  and involved in the adsorption process. According to the results of XRD analysis, the crystal structures of  $\text{Fe}_3\text{O}_4\text{/BIO-Cu}$  and  $\text{Fe}_3\text{O}_4\text{/BIO-Pb}$  mainly consisted

of  $\text{Cu}_2(\text{OH})_3\text{NO}_3$  and  $\text{PbCO}_3$ , respectively. So the chemical process with new substances being produced is the one of the adsorption mechanisms.

Loading  $\text{Fe}_3\text{O}_4$  conferred a larger BET surface area for BIO, making the  $\text{Cu}^{2+}$  adsorption capacity higher in a certain range while decreasing the  $\text{Pb}^{2+}$  adsorption capacity. However, as the weight ratio of  $\text{Fe}_3\text{O}_4$  increased, the adsorption capacity of  $\text{Fe}_3\text{O}_4\text{/BIO}$  for  $\text{Cu}^{2+}$  was declined and that for Pb further decreased. This mainly resulted from the coating of  $\text{Fe}_3\text{O}_4$  onto the BIO surface, which impeded the reaction between the surface of the adsorbent and heavy metals. Hence, it can be concluded that the adsorption mechanism for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  on  $\text{Fe}_3\text{O}_4\text{/BIO}$  was controlled by physical process and sharing with chemical process, but their relative weight may be different for different metals resulting in the different of adsorption characteristic shown as Fig. 1.

### 3.4. Regeneration, reuse, and comparison

The recycle and reuse performance of  $\text{Fe}_3\text{O}_4\text{/BIO}$  was studied to decrease the usage cost. In this study,  $\text{HNO}_3$  solution at pH 2.0 was used to conduct the regeneration. As shown in Fig. 9, both adsorption and recovery efficiency of  $\text{Fe}_3\text{O}_4\text{/BIO}$  gradually decreased with the increase in cycling times. After four times of regeneration (Fig. 9), the adsorption capacity of  $\text{Fe}_3\text{O}_4\text{/BIO}$  for both  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  remained at 45%–70% of its initial capacity and recovery efficiency. First, partly  $\text{Fe}_3\text{O}_4$  was dissolved from the BIO surface in the process of regeneration. Second,  $\text{H}^+$ , which has small hydrated radius, can replace ions such as  $\text{K}^+$ ,  $\text{Ca}^{2+}$ ,  $\text{Na}^+$ , and  $\text{Mg}^{2+}$  at the same time, thus lowering the ion-exchange

Table 4  
The binding energies of C, O, and Fe before and after adsorption

Sample	C 1s			O 1s			Fe 2p <sub>3/2</sub>
	C-C/C-H	C-O	O-O=C	O-C	O=C	O-H	
$\text{Fe}_3\text{O}_4\text{/BIO}$	284.83	286.40	289.59	531.49	532.18	532.99	712.45
$\text{Fe}_3\text{O}_4\text{/BIO-Cu}$	284.81	286.29	289.17	531.66	532.26	533.09	712.46
$\text{Fe}_3\text{O}_4\text{/BIO-Pb}$	284.81	286.15	289.22	531.30	532.20	533.20	712.45

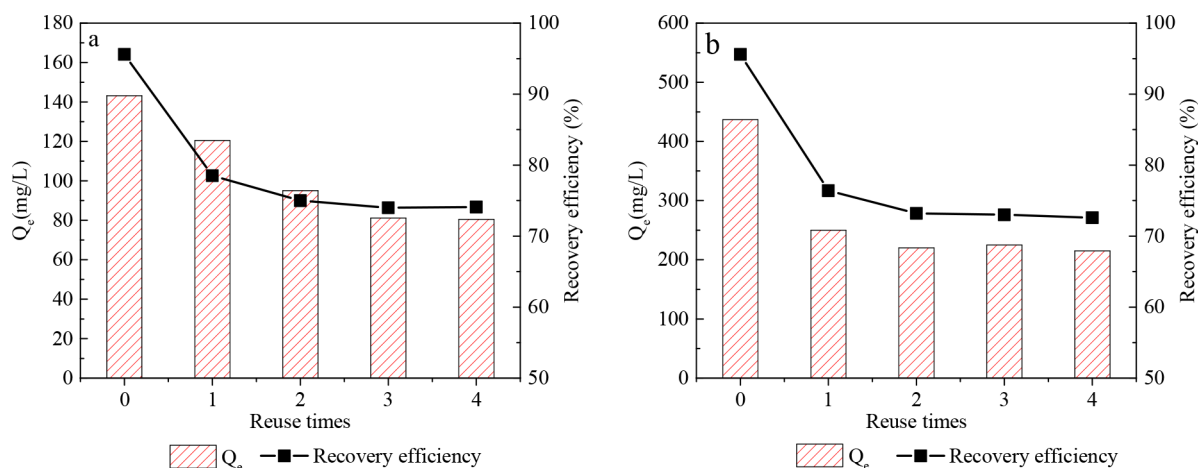


Fig. 9. The adsorption capacity ( $Q_e$ ) and recovery efficiency of  $\text{Fe}_3\text{O}_4\text{/BIO}$  in regeneration cycle for  $\text{Cu}^{2+}$  (a) and  $\text{Pb}^{2+}$  (b).

capacity. Furthermore, some crystal structures of  $\text{Fe}_3\text{O}_4\text{@BIO}$  may be destroyed under acidic conditions, especially carbonate, which can be dissolved and cannot be regenerated. These reasons explain the decline of the adsorption capacity and recovery efficiency of the  $\text{Fe}_3\text{O}_4\text{@BIO}$  composite.

There is a comparison of maximum adsorption capacities between the  $\text{Fe}_3\text{O}_4\text{@BIO}$  and other reports, and the results are presented in Table 5. The adsorption capacity of  $\text{Fe}_3\text{O}_4\text{@BIO}$  for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  is excellent, higher than that of other studies. Such comparison shows that  $\text{Fe}_3\text{O}_4\text{@BIO}$  synthesized by co-precipitation method is an efficient adsorbent for the treatment of wastewater with heavy-metal ions.

#### 4. Conclusion

In this study, a magnetic adsorbent was synthesized, and its properties were investigated by SEM, FTIR spectroscopy, XPS, and XRD.  $\text{Fe}_3\text{O}_4\text{@BIO}$  had an adsorption capacity for  $\text{Cu}^{2+}$  higher than that of BIO in a certain range of BIO/ $\text{Fe}_3\text{O}_4$  weight ratio but for  $\text{Pb}^{2+}$  that was lower. As the ratio continuously increased, both  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  adsorption capacity declined, while the BET surface area of the adsorbent and the separation behavior of the magnetic biochar increased. On the basis of these results, the optimum BIO/ $\text{Fe}_3\text{O}_4$  weight ratio was found to be 5:1 to 3:1. We used 3:1 in this study, for which the adsorption capability for  $\text{Cu}^{2+}$  was 143.2 mg/g and that for  $\text{Pb}^{2+}$  was 463.8 mg/g. The adsorption mechanisms for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  on  $\text{Fe}_3\text{O}_4\text{@BIO}$  were controlled by a physical process shared by a chemical process, but their relative weight may be different for different metals. Furthermore, the adsorption capacity could retain 60%–70% of the capacity after four times of regeneration and reuse. Overall, our magnetic bio-

char can be an alternative adsorbent for use in wastewater treatment processes because of their excellent heavy-metal adsorption ability and easy recovery after use. However, the regeneration process of the adsorbent method should be further studied to maintain good magnetic properties and heavy-metal adsorption capacity. This includes using different types and concentrations of regenerant and various regeneration processes.

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Table 5  
Comparison of adsorption capacities for  $\text{Cu}^{2+}$  and  $\text{Pb}^{2+}$  in various studies

Adsorbent	Modified method	$\text{Cu}^{2+}$ (mg/g)	$\text{Pb}^{2+}$ (mg/g)	References
Biochar	Magnetization	85.93	–	[25]
Biochar	–	11.34	–	[25]
Activated carbon	Phosphoric acid	19.6	–	[26]
Activated carbon	–	24.5	–	[26]
Biochar	–	56.1	–	This study
Biochar	Magnetization	143.2	–	This study
Biochar	Magnetization	–	52.4	[12]
Biochar	Magnetization	–	162.75	[13]
Activated carbon	–	–	99.5	[27]
Activated carbon	–	–	134.2	[28]
Biochar	–	–	665.4	This study
Biochar	Magnetization	–	463.8	This study

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